

White Bluff Steam Electric Station Plant Performance Group

December 2, 1992

Inter-Office Correspondence

TO:

Mr. Mickey Cox

FROM:

Dennis A. Wall

SUBJECT: 1992 Heat Rate Tests - White Bluff Units

Analysis of the subject tests has been completed, and the results are attached for your review. As in past years, the tests were conducted in accordance with the Entergy Heat Rate Test Procedure, and all co-owners were notified in advance so they could witness the tests. Only AECC chose to do so.

I believe the attached results are correct and representative of the present condition of these units. It is my recommendation that:

- 1. These results should be submitted to the System Operations Center, in order to update the economic dispatch curves for these units;
- 2. These results should be submitted to Mr. Alan Hardy, State Director of Bulk Power Marketing, for use in co-owner billing and related matters.

If you agree with my recommendations, please forward copies of the attachments to the parties mentioned above. If you disagree, please let me know so that we may otherwise resolve this issue. My telephone extension is 7021.

DAW/dw Attachments

cc: Mr. Max Halbert

Mr. Rick Perryman

Dr. Dale Swindle

Mr. Ron House

Mr. Roger Lawson

An Entergy Company

I and Cl W.

1992 Heat Rate Tests' Information White Bluff SES Unit 1

| Summer Corrected Net Generation | Heat Input |
|------------------------------------|--------------|
| (MW) | (MMBtu/Hr) |
| 144.14 | 2176.40 |
| 149.18 | 2227.80 |
| 236.26 | 3125.70 |
| 236.69 | 3142.80 |
| 333.00 | 3933.60 |
| 341.61 | 4037.90 |
| 429.51 | 4785.60 |
| 437.02 | 4791.30 |
| 519.98 | 5717.00 |
| 530.77 | 5721.40 |
| 607.67 | 6445.70 |
| 609.51 | 6417.30 |
| 707.54 | 7575.50 |
| 712.33 | 7398.60 |
| 792.43 | 8244.90 |
| 792.90 | 8369.70 |

Input/OutPut Equation:

Incremental Heat Rate Equation:

Incremental Heat Rate = (8.406449 + 0.001966 x NetMW) x 1000 = Btu/Net KwH

Net Heat Rate Equation:

Net Heat Rate = (1008.9797 + 8.406449 x NetMW + 0.000983 x NetMW²) x 1000/NetMW = Btu/Net KwH

1992 Heat Rate Tests' Information White Bluff SES Unit 2

| Summer Corrected Net Generation | Heat Input |
|------------------------------------|--------------|
| (MW) | (MMBtu/Hr) |
| 172.15 | 2315.30 |
| 175.64 | 2320.70 |
| 255.07 | 3019.50 |
| 255.88 | 3015.70 |
| 354.48 | 4010.00 |
| 360.93 | 4010.10 |
| 450.76 | 4902.00 |
| 454.69 | 4922.50 |
| 548.60 | 5769.90 |
| 550.80 | 5746.70 |
| 659.57 | 6853.40 |
| 666.80 | 6832.20 |
| 737.57 | 7530.90 |
| 748.18 | 7620.30 |
| 824.33 | 8528.00 |
| 829.40 | 8559.60 |

Input/OutPut Equation:

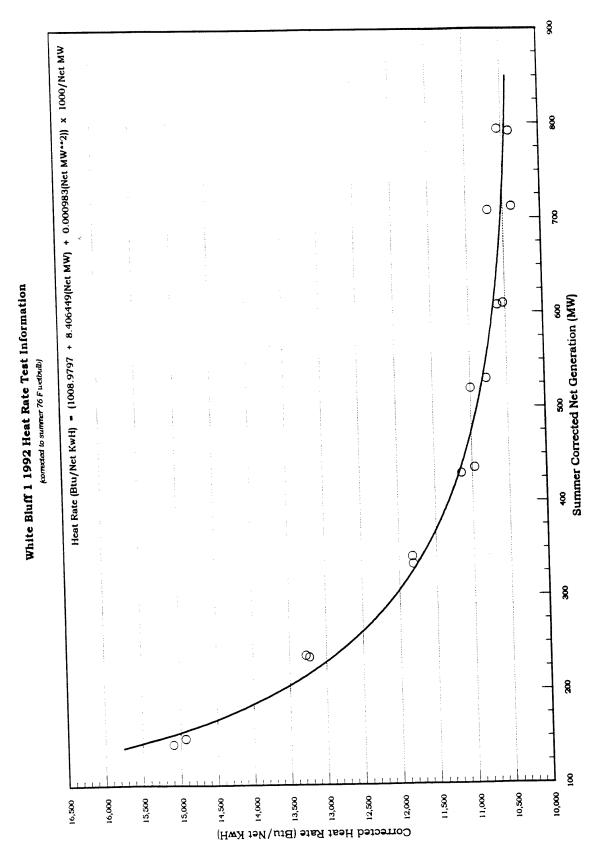
Heat Input = 811.6667 + 8.529974 x NetMW + 0.000904 x NetMW²
= MMBtu/Hr

Incremental Heat Rate Equation:

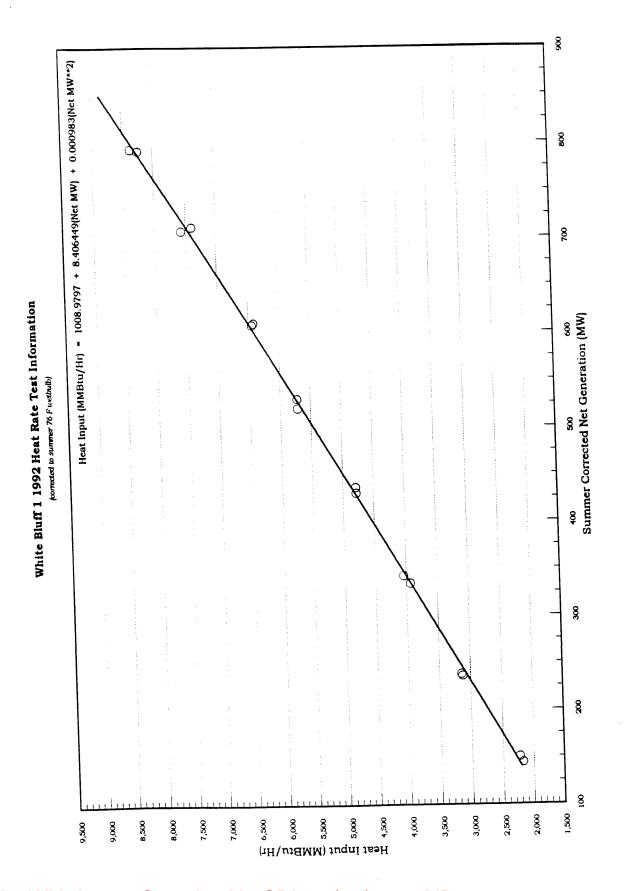
Incremental Heat Rate = (8.529974 + 0.001808 x NetMW) x 1000 = Btu/Net KwH

Net Heat Rate Equation:

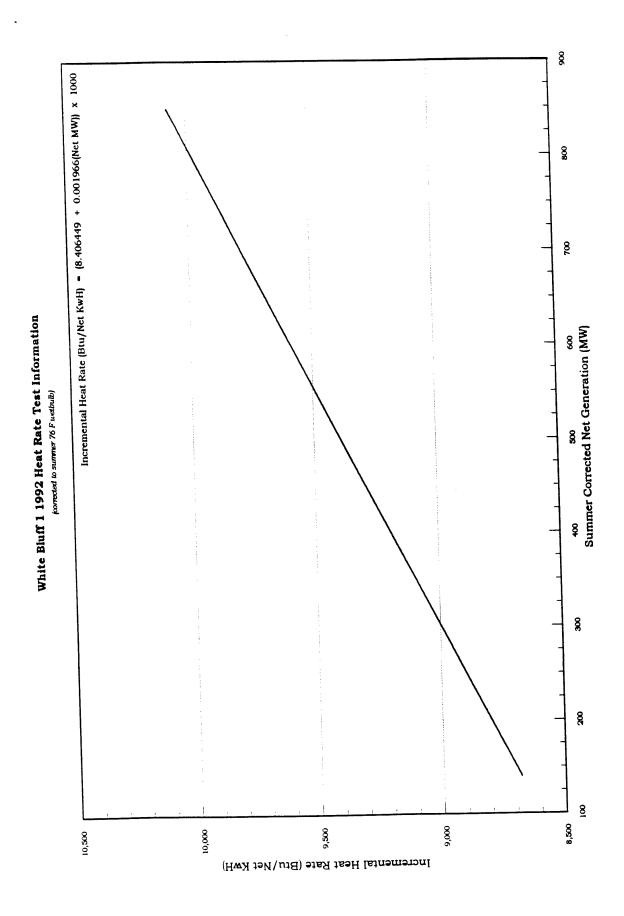
Net Heat Rate = (811.6667 + 8.529974 x NetMW + 0.000904 x NetMW ²) x 1000/NetMW = Btu/Net KwH

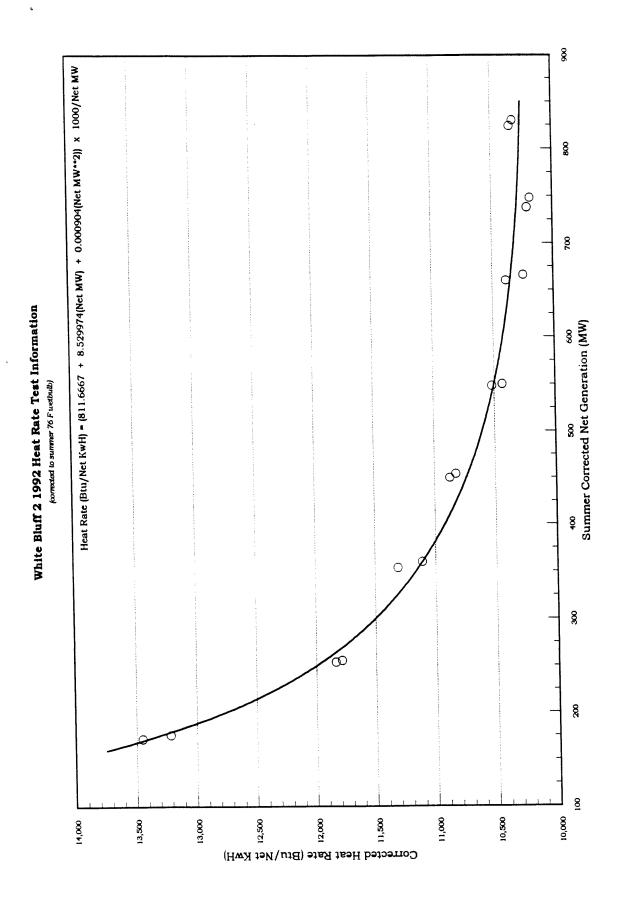


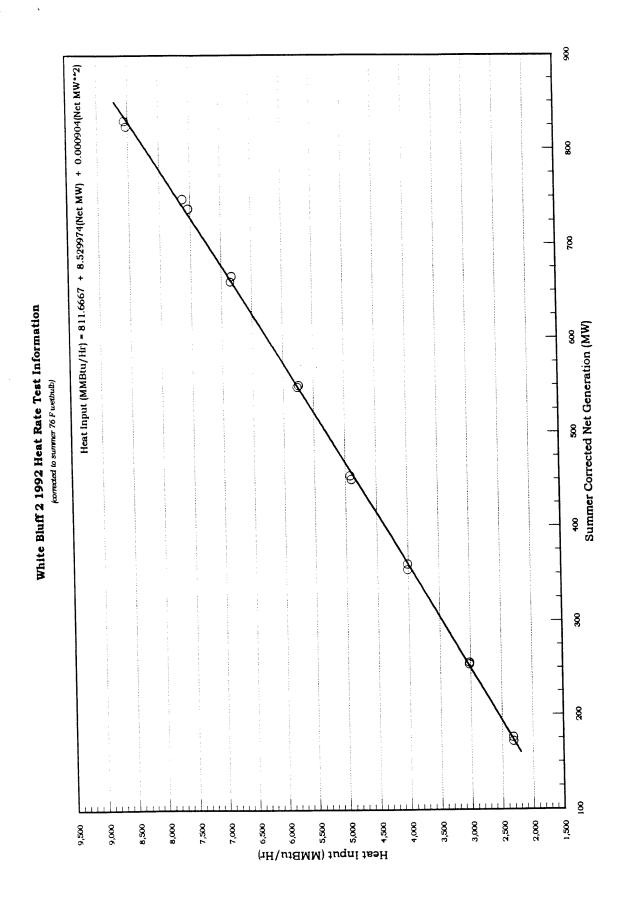
Claim Withdrawn. Contains No CBI. 06/29/2016_YD



Claim Withdrawn. Contains No CBI. 06/29/2016_YD







Incremental Heat Rate (Btu/Net KwH) = (8.529974 + 0.001808(Net MW)) x 1000 8 8 White Bluff 2 1992 Heat Rate Test Information 400 500 600 Summer Corrected Net Generation (MW) (corrected to summer 76 F wetbulb) 8 8 8 10,000 Incremental Heat Rate (Btu/ Net KwH)

8



June 28, 1993

mer-Office Correspondence

TO:

Mr. Mickey Cox

FROM:

Dennis A. Wall

Senior Engineer, Diagnostic Services Section

SUBJECT: 1993 Heat Rate Test Results - White Bluff Unit 1

White Bluff Unit 1 was tested the week of May 16. The calculations and evaluation of results have just now been completed, and the results are attached for your review. For your convenience, 1992's results are also included. As always, these tests were run in an unbiased manner in accordance with the Entergy test procedure. Co-owners were notified prior to the tests, and engineers from the Arkansas Electric Co-operative Corporation were present for every test.

The significant difference between the 1992 and 1993 curves is primarily explained by the fact that the unit is operating with the "A" train of high pressure feedwater heaters isolated due to a tube leak in the 2A heater. This heater is scheduled for replacement during the Fall, 1993 outage, after which it would be appropriate to retest this unit with all heaters in service. Until then, it is my recommendation that the 1993 results be implemented immediately for dispatch and co-owner billing purposes, since they best represent the present condition of the unit.

If you need any additional information, or if you have any comments, please do not hesitate to contact me at telephone extension 7021.

Denno a. Wall

DAW/dw Attachments

cc: Mr. Max Halbert

Mr. Ron House

Mr. Art Gilreath

Mr. William Phillips

Mr. Alan Hardy

Mr. John Harrison

Mr. Gary Davis

1993 Heat Rate Tests' Information White Bluff SES Unit 1

| Summer Corrected Net Generation | Heat Input |
|------------------------------------|--------------|
| (MW) | (MMBtu/Hr) |
| 150.12 | 2252.60 |
| 150.91 | 2245.50 |
| 239.13 | 3062.10 |
| 239.67 | 3079.10 |
| 333.87 | 3936.40 |
| 338.84 | 3894.90 |
| 439.54 | 4903.20 |
| 439.84 | 4856.50 |
| 545.93 | 5900.50 |
| 546.36 | 5897.10 |
| 633.85 | 6813.50 |
| 641.74 | 6853.00 |
| 736.30 | 7962.90 |
| 737.21 | 8047.20 |
| 784.42 | 8484.40 |
| 790.07 | 8559.20 |

Input/OutPut Equation:

Heat Input = $1103.9930 + 7.461433 \times \text{NetMW} + 0.002501 \times \text{NetMW}^2$ = MMBtu/Hr

Incremental Heat Rate Equation:

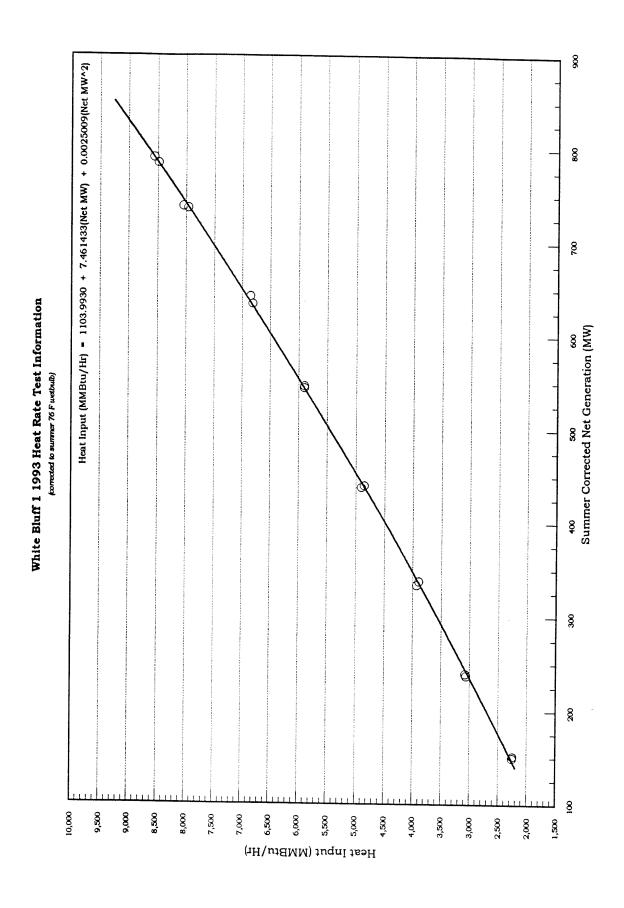
Incremental Heat Rate = (7.461433 + 0.005002 x NetMW) x 1000 = Btu/Net KwH

Net Heat Rate Equation:

Net Heat Rate = $(1103.9930 + 7.461433 \text{ x NetMW} + 0.002501 \text{ x NetMW}^2) \times 1000/\text{NetMW}$ = Btu/Net KwH

8 Corrected Heat Rate (Btu/Net KwH) = (1103.9930 + 7.461433(Net MW) + 0.0025009(Net MW^2)) x 1000 / Net MW 8 8 B White Bluff 1 1993 Heat Rate Test Information 400 500 600 Summer Corrected Net Generation (MW) (corrected to summer 76 F wetbulb) 8 8 15,500 15,000 14,500 11,000 10,500 10,000

Corrected Heat Rate (Btu/Net KwH)



8 Incremental Heat Rate (Btu/Net KwH) = (7.461433 + 0.0050018(Net MW)) x 1000 800 8 White Bluff 1 1993 Heat Rate Test Information 400 500 600 Summer Corrected Net Generation (MW) (corrected to summer 76 F weabulb.) 8 8 8 12,000 11,500 11,000 8,500 8,000 7,500 Incremental Heat Rate (Btu/Net KwH)



August 16, 1993

nter-Office Correspondence

TO:

Mr. Mickey Cox

FROM:

Dennis A. Wall

Senior Engineer, Diagnostic Services Section

SUBJECT:

1993 Heat Rate Test Results - White Bluff Unit 2

White Bluff Unit 2 was tested the week of June 21. One test load was repeated on July 14. The calculations, evaluation, and review of results have now been completed, and the results are attached for your review. For your convenience, a graphical comparison with 1992's results are also included. As always, these tests were run in an unbiased manner in accordance with the Entergy test procedure. Co-owners were notified prior to the tests, and engineers from the Arkansas Electric Co-operative Corporation were present.

Although slight, there is some difference between the 1992 and 1993 curves. It is my recommendation that the 1993 results be implemented immediately for dispatch and co-owner billing purposes, since they best represent the present condition of the unit.

If you need any additional information, or if you have any comments, please do not hesitate to contact me at telephone extension 7021.

Dennis a. Wall

DAW/dw Attachments

cc: Mr. Max Halbert

Mr. Ron House

Mr. Art Gilreath

Mr. William Phillips

Mr. Alan Hardy

Mr. John Harrison

Mr. Gary Davis

1993 Heat Rate Tests' Information White Bluff SES Unit 2

| Summer Corrected Net Generation | Heat Input |
|------------------------------------|--------------|
| (MW) | (MMBtu/Hr) |
| 164.96 | 2253.00 |
| 165.97 | 2245.10 |
| 255.32 | 3007.00 |
| 260.63 | 3044.70 |
| 364.01 | 4050.50 |
| 366.32 | 4068.70 |
| 462.78 | 4941.80 |
| 465.00 | 4920.50 |
| 558.13 | 5830.70 |
| 558.64 | 5815.80 |
| 654.56 | 6734.00 |
| 654.81 | 6729.70 |
| 753.60 | 7798.60 |
| 756.57 | 7809.60 |
| 811.60 | 8329.10 |
| 814.39 | 8338.20 |

Input/OutPut Equation:

Heat Input = $842.7447 + 8.268214 \times \text{NetMW} + 0.001187 \times \text{NetMW}^2$ = MMBtu/Hr

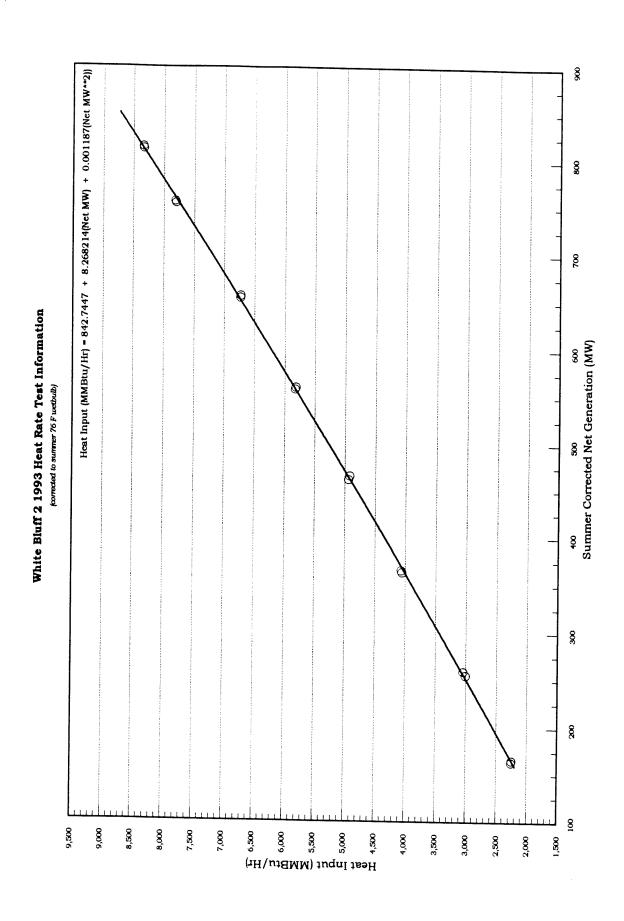
Incremental Heat Rate Equation:

Incremental Heat Rate = (8.268214 + 0.002374 x NetMW) x 1000 = Btu/Net KwH

Net Heat Rate Equation:

Net Heat Rate = (842.7447 + 8.268214 x NetMW + 0.001187 x NetMW ²) x 1000/NetMW = Btu/Net KwH

8 Heat Rate (Btu/Net KwH) = (842.7447 + 8.268214(Net MW) + 0.001187(Net MW**2)) x 1000/Net MW 8 8 White Bluff 2 1993 Heat Rate Test Information 400 500 600 Summer Corrected Net Generation (MW) (corrected to summer 76 F wetbulb) 8 8 8 14,000 13,500 13,000 10,500 10,000 Corrected Heat Rate (Btu/Net KwH)



8 Incremental Heat Rate (Btu/Net KwH) = (8.268214 + 0.002374 x Net MW) x 1000 700 White Bluff 2 1993 Heat Rate Test Information 400 500 600 Summer Corrected Net Generation (MW) (corrected to summer 76 F wetbulb) 000'6 8,500

Incremental Heat Rate (Btu/Net KwH)



January 16, 1995

Inter-Office Correspondence

TO:

Mr. Mike Bakewell

FROM:

Ron House

SUBJECT:

1994 Heat Rate Tests - White Bluff Plant

White Bluff Unit Heat Rate tests were conducted in August and September of last year. An analysis of the tests and their results is attached for your review. As in past years, the tests were conducted in an unbiased manner and in accordance with the Entergy Heat Rate Test Procedure. All White Bluff co-owners were notified in advance so they could witness the tests. Engineers from Arkansas Electric Co-operative were present and participated in the testing.

Please note that there are some differences between the 1993 and 1994 test results:

Unit 1 had a slight overall improvement over 1993. This is primarily due to cooling tower repairs performed in the 1994 spring outage. However, the unit heat rate is still considerably higher than desired. The "B" train of high pressure heaters remains isolated due to tube failures in the 2"B" heater. This heater will be replaced during the 1995 spring boiler outage. The replacement will significantly improve unit heat rate and it would be appropriate then to retest the unit with all heaters in service.

Unit 2 had a notable degradation from 1993. The two primary causes are 1) a plugged air pre-heater and 2) high pressure heater train "A" being isolated due to tube failures in the 2"A" high pressure heater. A number of repairs have been made to the feedwater heater with subsequent additional failures. It remains out of service at this time. Heat rate will be impacted by these conditions, along with a potential limit to unit capacity during summer operation.

I believe the attached results are correct and representative of the present condition of the units. It is my recommendation that these results be implemented for dispatch and co-owner billing purposes. Please pardon the delay in completing this task. It is possible that the co-owners will wish to back calculate fuel costs for November and December. If you need any additional information or if you have any comments, please do not hesitate to contact me at extension 7009.

Fon House

RHH/rh

w/Attachments

cc: Mr. Henry Thompson A-TCBY-23-G

Mr. David Harris AECC

Mr. Art Gilreath T-EP-16

Mr. William C. Phillips ... A-SOC/PB

Mr. Lynn Sanders

Mr. Rick Perryman

dr. Tom Odenthall

Mr. Nate Stephens

Mr. Jim Booth

Mr. Mike Charles

Mr. Wayne Webb

Mr. Pat Klepper A-ISES

1994 Heat Rate Tests' Information White Bluff SES Unit 1

| ummer Corrected Net Generation | Heat Input |
|-----------------------------------|--------------|
| | |
| (MW) | (MMBtu/Hr) |
| 159.76 | 2312.70 |
| 160.39 | 2386.70 |
| 243.34 | 3143.20 |
| 249.42 | 3158.20 |
| 340.75 | 3972.90 |
| 344.93 | 3982.90 |
| 455.18 | 4895.80 |
| 446.57 | 4939.00 |
| 547.84 | 5946.00 |
| 555.13 | 5915.50 |
| 636.64 | 6786.40 |
| 648.98 | 6824.00 |
| 754.00 | 8031.10 |
| 755.00 | 8010.20 |
| 791.13 | 8225.90 |
| 785.33 | 8266.00 |

Input/OutPut Equation:

Incremental Heat Rate Equation:

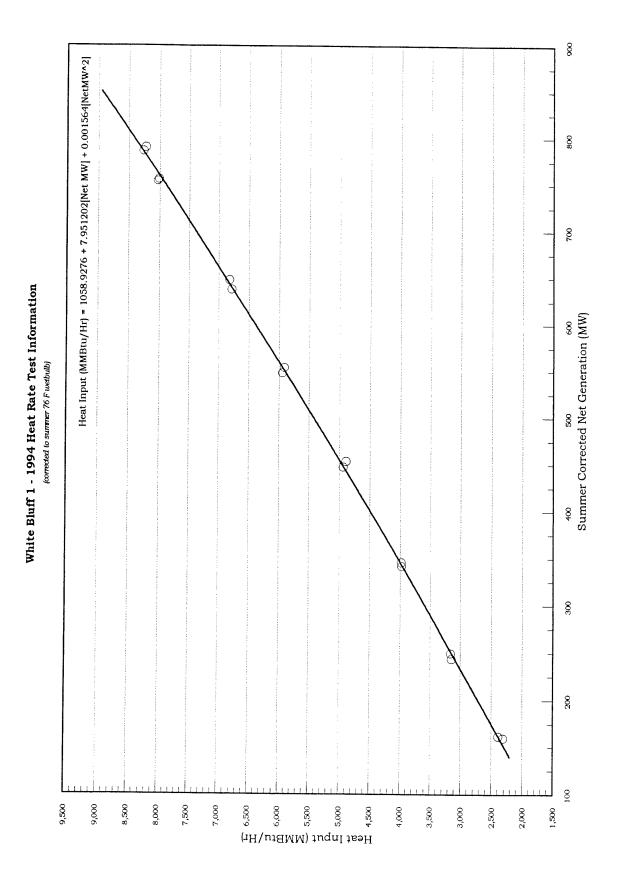
Incremental Heat Rate =
$$(7.951202 + 0.003128 \times NetMW) \times 1000$$

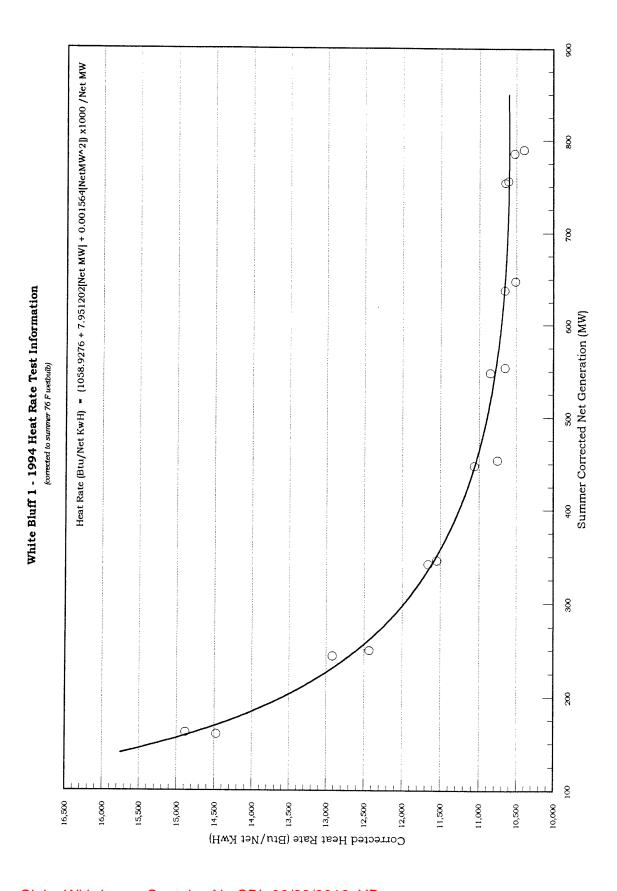
= Btu/Net KwH

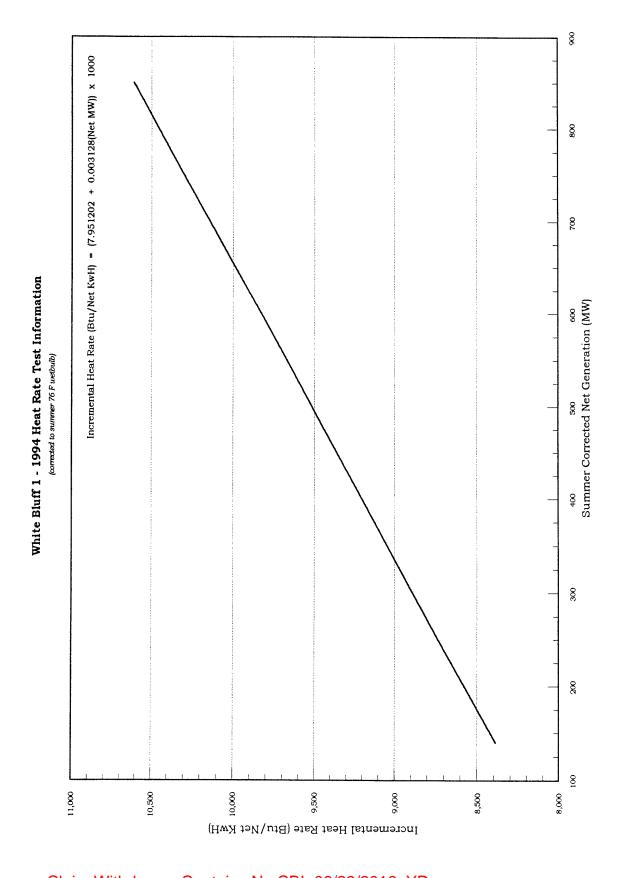
Net Heat Rate Equation:

Net Heat Rate =
$$(1058.9276 + 7.951202 \text{ x NetMW} + 0.001564 \text{ x NetMW}^2) \text{ x } 1000/\text{NetMW}$$

= Btu/Net KwH







HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 160MW 1ST HR

| MEASURED TEST INPUTS FROM FILE wb1hr94a.160 | |
|--|--|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS 95.36 THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| THE AVERAGE OIL HIGH HEATING VALUE IS | BIU/BBL |
| | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| THE DESIGN COLD WATER TEMPERATURE IS | DEG F |
| THE AVERAGE MAXIMUM CONDENSER COOLING WATER | |
| TEMPERATURE IS | |
| CONDENSER COOLING WATER TEMPERATURE IS 2.14 THE TURBINE THROTTLE FLOW IS | IN-HG LB/HR |
| THE HEAT RATE CORRECTION FACTOR FOR CONDENSER BACKPRESSURE IS14.89 | 8 |
| THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | · |
| PRESSURE IS12.83 BPCHG = 2.42 | 8 |
| KWCHG = -2.37 | _ |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.023651 | |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 14084.4 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 14475.4 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 160MW 2ND HR

| MEASURED TEST INPUTS FROM FILE WB1HR94B.160 | |
|--|---|
| THE AVERAGE GROSS GENERATION IS | MMa |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| THE AVERAGE OIL FLOW IS | BRI./HR |
| CALCULATED RESULTS | through the second |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | IN-HG LB/HR |
| BACKPRESSURE IS15.14 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM | % |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS12.87 BPCHG = 2.68 KWCHG = -2.61 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.026084 | % |
| THE CORRECTED GROSS GENERATION IS 188.09 | MWe |
| THE CORRECTED NET GENERATION IS 160.39 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 14438.8 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 14880.5 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 2386.7 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 250MW 1ST HR

| MEASURED TEST INPUTS FROM FILE wb1hr94a.250 | |
|---|-------------------------|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE CONDENSER IS | DEG F DEG F DEG F |
| THE COMPUTED RELATIVE HUMIDITY IS | LB/HR BTU/LB |
| THE INVENTIGE OF MICH MEMITING VINEER TO | DIO/DDD |
| | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | |
| BACKPRESSURE IS11.27 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM | % |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS9.71 BPCHG = 1.75 KWCHG = -1.72 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.017229 | % |
| THE CORRECTED GROSS GENERATION IS 270.34 | MWe |
| THE CORRECTED NET GENERATION IS 243.34 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 12674.1 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 12916.7 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 250MW 2ND HR

| MEASURED TEST INPUTS FROM FILE wb1hr94b.250 | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | 4 |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F IN-HG LB/HR |
| | |
| THE CORRECTED GROSS GENERATION IS | |
| THE CORRECTED NET GENERATION IS 249.42 | |
| THE UNCORRECTED NET HEAT RATE IS 12433.7 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 12661.8 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 350MW 1ST HR

| MEASURED TEST INPUTS FROM FILE wb1hr94a.350 | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F IN-HG |
| THE HEAT RATE CORRECTION FACTOR FOR CONDENSER BACKPRESSURE IS8.47 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM | 8 |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS6.89 BPCHG = 1.72 KWCHG = -1.70 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.016957 | ४ |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 11449.3 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 11659.4 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 350MW 2ND HR

| MEASURED TEST INPUTS FROM FILE wb1hr94b.350 | |
|--|-------------------|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F |
| THE AVERAGE COAL FLOW IS | LB/HR BTU/LB |
| THE AVERAGE OIL FLOW IS | BBL/HR BTU/BBL |
| | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| TEMPERATURE IS | |
| CONDENSER COOLING WATER TEMPERATURE IS | LB/HR |
| BACKPRESSURE IS8.55 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | % |
| PRESSURE IS7.04 BPCHG = 1.65 KWCHG = -1.62 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.016227 | % |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 11547.0 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 450MW 1ST HR

| MEASURED TEST INPUTS FROM FILE wb1hr94a.450 | |
|--|--|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HP |
| | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | IN-HG LB/HR |
| BACKPRESSURE IS6.17 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | 8 |
| PRESSURE IS5.06 BPCHG = 1.19 KWCHG = -1.17 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.011717 | % |
| THE CORRECTED GROSS GENERATION IS 488.28 | MWe |
| THE CORRECTED NET GENERATION IS 455.18 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10622.2 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10755.7 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 4895.8 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 450MW 2ND HR

| MEASURED TEST INPUTS FROM FILE wb1hr94b.450 | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F IN-HG LB/HR |
| BPCHG = 0.96 KWCHG = -0.95 THE BACKPRESSURE CORRECTION FACTOR IS 1.009491 | % |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10948.8 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 11059.9 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 550MW 1ST HR

| MEASURED TEST INPUTS FROM FILE wb1hr94a.550 | |
|--|----------------|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE | |
| CONDENSER IS | DEG F DEG F |
| THE AVERAGE COAL FLOW IS | T.R / HD |
| THE AVERAGE OIL FLOW IS | BBI./HD |
| THE AVERAGE OIL HIGH HEATING VALUE IS | BTU/BBL |
| | ···· |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | IN-HG |
| THE HEAT RATE CORRECTION FACTOR FOR CONDENSER | • |
| BACKPRESSURE IS4.22 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | % |
| PRESSURE IS3.53 BPCHG = 0.72 KWCHG = -0.71 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.007130 | % |
| THE CORRECTED GROSS GENERATION IS 582.84 | MWe |
| THE CORRECTED NET GENERATION IS 547.84 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10771.7 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10853.4 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 5946.0 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 550MW 2ND HR

| MEASURED TEST INPUTS FROM FILE wb1hr94b.550 | |
|--|--|
| THE AVERAGE GROSS GENERATION IS | MWA |
| CONDENSER IS 110.98 THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE | |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F |
| TEMPERATURE IS | IN-HG |
| THE TURBINE THROTTLE FLOW IS | • |
| BACKPRESSURE IS4.06 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | * |
| PRESSURE IS3.59 BPCHG = 0.49 KWCHG = -0.49 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.004893 | % |
| THE CORRECTED GROSS GENERATION IS 587.13 | MWe |
| THE CORRECTED NET GENERATION IS 555.13 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10601.2 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10656.1 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 650MW 1ST HR

| MEASURED TEST INPUTS FROM FILE wb1hr94a.650 | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | IN-HG LB/HR |
| BACKPRESSURE IS3.01 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM | % |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS2.23 BPCHG = 0.80 KWCHG = -0.80 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.007954 | % |
| THE CORRECTED GROSS GENERATION IS 673.64 | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10570.7 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10659.7 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 650MW 2ND HR

| MEASURED TEST INPUTS FROM FILE wb1hr94b.650 | |
|--|--|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HP |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | IN-HG LB/HR |
| BACKPRESSURE IS2.67 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | % |
| PRESSURE IS2.09 BPCHG = 0.59 KWCHG = -0.59 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.005890 | % |
| THE CORRECTED GROSS GENERATION IS 681.98 | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10450.3 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10514.9 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 750MW 1ST HR

| MEASURED TEST INPUTS FROM FILE wb1hr94a.750 | |
|--|--|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F |
| TEMPERATURE IS | IN-HG |
| BACKPRESSURE IS1.31 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | % |
| PRESSURE IS1.31 BPCHG = 0.00 KWCHG = 0.00 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.000000 | % |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10651.4 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10651.4 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 - 750MW 2ND HR

| MEASURED TEST INPUTS FROM FILE wb1hr94b.750 | |
|--|--------------------------------|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | |
| CONDENSER IS | DEG F DEG F PCT LB/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F |
| TEMPERATURE IS | |
| CONDENSER COOLING WATER TEMPERATURE IS | LB/HR |
| BACKPRESSURE IS1.14 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | % |
| PRESSURE IS1.14 BPCHG = 0.00 KWCHG = 0.00 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.000000 | 8 |
| THE CORRECTED GROSS GENERATION IS 791.00 | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10609.5 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10609.5 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 8010.2 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 1 FULL LOAD 1ST HR

| MEASURED TEST INPUTS FROM FILE wb1hr94a.815 | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS 122.32 THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE | |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| TEMPERATURE IS | |
| CONDENSER COOLING WATER TEMPERATURE IS | IN-HG LB/HR |
| BACKPRESSURE IS0.82 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMIM | % |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.001045 | % |
| THE CORRECTED GROSS GENERATION IS 828.13 | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10386.2 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10397.6 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 8225.9 | MMBTU |
| | |

HEAT RATE CORRECTIONS FOR ...HITE BLUFF UNIT 1 FULL LOAD 2ND HR

| MEASURED TEST INPUTS FROM FILE wb1hr94b.815 |
|---|
| THE AVERAGE GROSS GENERATION IS |
| THE AVERAGE CIRCULATING WATER TEMPERATURE FROM THE CONDENSER IS |
| THE AVERAGE AMBIENT WET BULB TEMPERATURE IS |
| THE AVERAGE COAL HIGH HEATING VALUE IS |
| CALCULATED RESULTS |
| THE COOLING TOWER CIRCULATING WATER FLOW IS |
| THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS |
| CONDENSER COOLING WATER TEMPERATURE IS |
| THE HEAT RATE CORRECTION FACTOR FOR CONDENSER BACKPRESSURE IS |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS1.18 % BPCHG = 0.08 |
| KWCHG = -0.08 THE BACKPRESSURE CORRECTION FACTOR IS 1.000819 % |
| THE CORRECTED GROSS GENERATION IS 821.33 MWe |
| THE CORRECTED NET GENERATION IS |
| THE UNCORRECTED NET HEAT RATE IS 10516.5 BTU/NKW |
| THE CORRECTE NET HEAT RATE IS 10525.5 BTU/NKW |
| THE TOTAL HENT INPUT IS 8266.0 MMBTU |

----- REGRESSION ANALYSIS -----HEADER DATA FOR: E:WB1HR94 LABEL: WHITE BLUFF UNIT 1 HEAT RATE TESTS 1994 NUMBER OF CASES: 16 NUMBER OF VARIABLES: 3 INDEX NAME MEAN STD.DEV. 1 CNM 492.1493750 224.3437909 2 CNM² 289395.5106250 219997.5571325 DEP. VAR.: HEATIN 5424.7812500 2124.1648810 DEPENDENT VARIABLE: HEATIN VAR. REGRESSION COEFFICIENT STD. ERROR T(DF=13)PARTIAL r^2 PROB. CNM 7.9512023 .4029996 19.730 .00000 .9677 CNM² .0015642 .0004110 3.806 .00218 .5271 CONSTANT 1058.9275623 STD. ERROR OF EST. = 61.8466702ADJUSTED R SQUARED = .9991523 R SQUARED = .9992653 MULTIPLE R = .9996326 ANALYSIS OF VARIANCE TABLE SOURCE SUM OF SQUARES D.F. MEAN SQUARE F RATIO PROB. REGRESSION 67631421.4863450 2 33815710.7431730 8840.684 .000E+00 RESIDUAL 49725.1380312 13 3825.0106178 TOTAL 67681146.6243760 15 STANDARDIZED RESIDUALS OBSERVED RESIDUAL -2.0 CALCULATED 2.0 2312.700 2369.135 -56.435304 2386.700 2374.460 12.239954 3 3143.200 3086.397 56.803358 3158.200 3139.426 18.773715 5 3972.900 3949.921 22.979315 б 3982.900 3987.640 -4.739947 * 7 4895.800 5002.242 -106.442019 8 4939.000 4921.638 17.362444 5946.000 5884.378 61.622442 10 5915.500 5954.919 **-**39.419063 11 6786.400 6754.970 31.429555 12 6824.000 6877.904 -53.903719 13 8031.100 7943.411 87.689278 14 7953.722 8010.200 56.477687

DURBIN-WATSON TEST = 2.3221

8328.378

8267.959

8225.900

8266.000

15

-102.478474

-1.959222

1994 Heat Rate Tests' Information White Bluff SES Unit 2

| ummer Corrected Net Generation | Heat Input |
|-----------------------------------|--------------|
| (MW) | (MMBtu/Hr) |
| 162.15 | 2274.60 |
| 158.12 | 2268.50 |
| 246.15 | 3037.10 |
| 250.24 | 3059.30 |
| 353.24 | 4048.00 |
| 356.58 | 3997.90 |
| 456.57 | 4867.80 |
| 451.73 | 4889.00 |
| 556.54 | 5818.30 |
| 549.26 | 5829.00 |
| 656.20 | 6761.30 |
| 648.35 | 6720.80 |
| 755.23 | 7900.80 |
| 759.40 | 7929.30 |
| 836.53 | 8788.80 |
| 842.81 | 8716.00 |

Input/OutPut Equation:

Heat Input =
$$1015.5475 + 7.710367 \times \text{NetMW} + 0.001783 \times \text{NetMW}^2$$

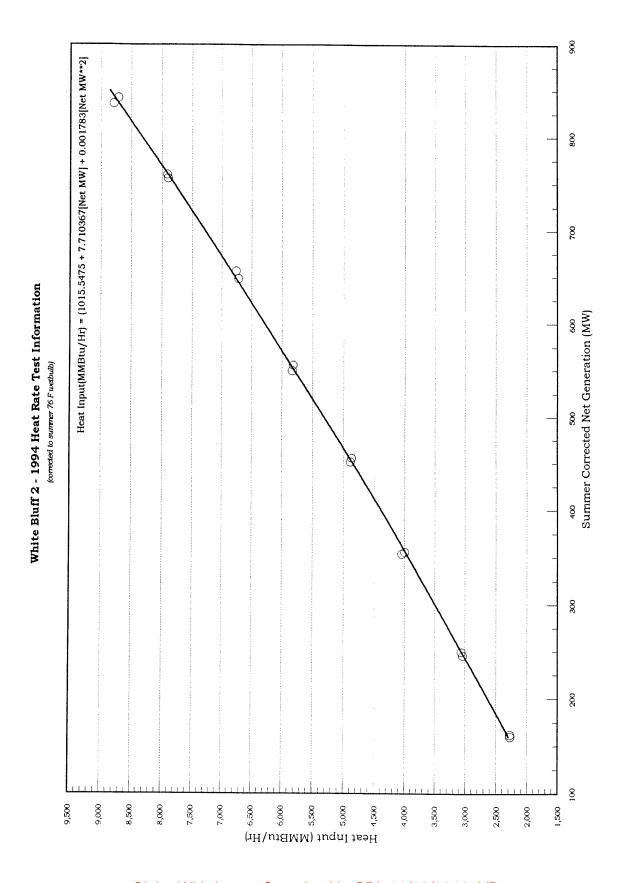
= MMBtu/Hr

Incremental Heat Rate Equation:

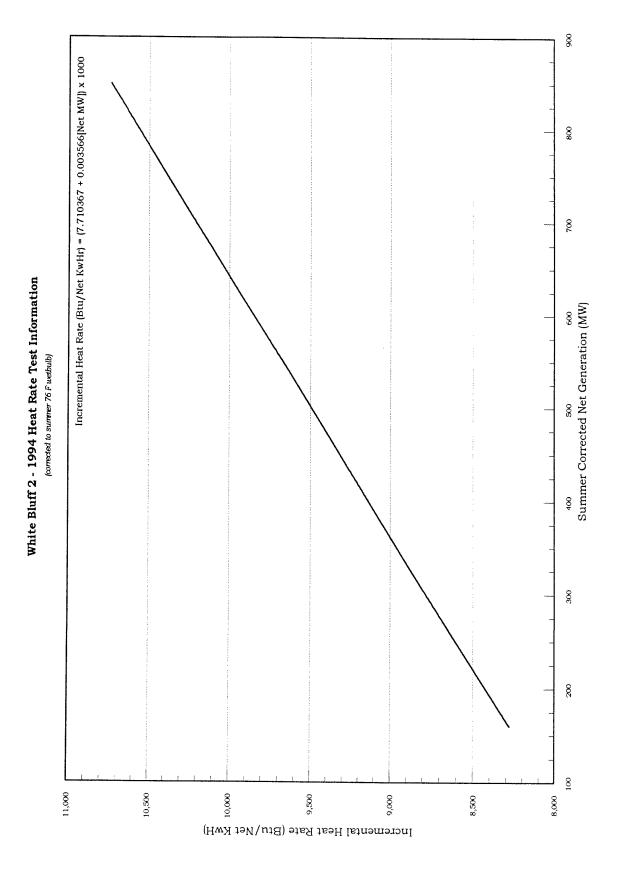
Incremental Heat Rate =
$$(7.710367 + 0.003566 x NetMW) x 1000$$

= Btu/Net KwH

Net Heat Rate Equation:



8 Heat Rate (Btu/Net KwHr) = (1015.5475 + 7.710367[Net MW] + 0.001783[Net MW**2]) x 1000/Net MW Ó 8 8 White Bluff 2 - 1994 Heat Rate Test Information 400 500 600 Summer Corrected Net Generation (MW) (corrected to summer 76 F wetbulb) 8 80 14,500 14,000 13,500 11,500 11,000 10,000 10,500 Corrected Heat Rate (Btu/Net KwH)



HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 160 - 1ST HR

| MEASURED TEST INPUTS FROM FILE wb2hr94a.160 | |
|--|--|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F |
| TEMPERATURE IS | IN-HG |
| THE HEAT RATE CORRECTION FACTOR FOR CONDENSER BACKPRESSURE IS17.00 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSED COOLING HAMED MEMORPHONE CAMBURATION | % |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS15.60 BPCHG = 1.68 KWCHG = -1.66 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.016561 | % |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 13768.6 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 14027.2 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 2274.6 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 160 - 2ND HR

| MEASURED TEST INPUTS FROM FILE wb2hr94b.160 | |
|--|--|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F IN-HG LB/HR |
| BPCHG = 1.86 KWCHG = -1.82 THE BACKPRESSURE CORRECTION FACTOR IS | 8 |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS 158.12 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 14055.3 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 14346.6 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 2268.5 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 250 - 1ST HR

| MEASURED TEST INPUTS FROM FILE wb2hr94a.250 | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F |
| TEMPERATURE IS | IN-HG |
| BACKPRESSURE IS13.01 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | % |
| PRESSURE IS11.64 BPCHG = 1.57 KWCHG = -1.54 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.015433 | % |
| THE CORRECTED GROSS GENERATION IS 268.85 | MWe |
| THE CORRECTED NET GENERATION IS 246.15 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 12133.8 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 12338.3 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 250 - 2ND HR

| MEASURED TEST INPUTS FROM FILE wb2hr94b.250 | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS 92.97 THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE | |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | LB/HR |
| BACKPRESSURE IS13.18 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | |
| PRESSURE IS12.16 BPCHG = 1.18 KWCHG = -1.16 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.011617 | % |
| THE CORRECTED GROSS GENERATION IS 271.84 | MWe |
| THE CORRECTED NET GENERATION IS 250.24 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 12072.8 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 12225.2 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 3059.3 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 350 - 1ST HR

| MEASURED TEST INPUTS FROM FILE wb2hr94a.350 | |
|--|--|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F |
| TEMPERATURE IS | IN-HG |
| THE HEAT RATE CORRECTION FACTOR FOR CONDENSER BACKPRESSURE IS8.97 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | 8 |
| PRESSURE IS8.52 BPCHG = 0.50 KWCHG = -0.49 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.004934 | % |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 11399.6 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 11459.6 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 350 - 2ND HR

| MEASURED TEST INPUTS FROM FILE wb2hr94b.350 | · · · · · · · · · · · · · · · · · · · |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HP |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | IN-HG LB/HR |
| BACKPRESSURE IS8.66 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM | 8 |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS8.32 BPCHG = 0.38 KWCHG = -0.37 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.003738 | % |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 11167.3 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 11211.8 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 450 - 1ST HR

| MEASURED TEST INPUTS FROM FILE wb2hr94a.450 | |
|--|--|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS 102.39 THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE | |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| THE AVERAGE OIL HIGH HEATING VALUE IS | BIO/BBL |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | IN-HG LB/HR |
| BACKPRESSURE IS6.87 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | 8 |
| PRESSURE IS6.56 BPCHG = 0.34 KWCHG = -0.34 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.003386 | % |
| THE CORRECTED GROSS GENERATION IS 481.37 | MWe |
| THE CORRECTED NET GENERATION IS 456.57 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10623.7 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10661.6 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 4867.8 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 450 - 2ND HR

| MEASURED TEST INPUTS FROM FILE wb2hr94b.450 | |
|---|-------------------------------------|
| THE AVERAGE GROSS GENERATION IS | MWa |
| CONDENSER IS 102.85 THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE | |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F |
| THE SATURATION PRESSURE FOR THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS | TN-HG |
| BACKPRESSURE IS6.89 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM | % |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS6.54 BPCHG = 0.37 KWCHG = -0.37 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.003724 | 8 |
| THE CORRECTED GROSS GENERATION IS 475.23 | MWe |
| THE CORRECTED NET GENERATION IS 451.73 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10780.6 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10822.8 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 550 - 1ST HR

| MEASURED TEST INPUTS FROM FILE wb2hr94a.550 | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWA |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F IN-HG LB/HR |
| THE CORRECTED GROSS GENERATION IS 584.34 | MWe |
| THE CORRECTED NET GENERATION IS 556.54 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10423.3 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10454.3 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 5818.3 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 550 - 2ND HR

| MEASURED TEST INPUTS FROM FILE wb2hr94b.550 | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F IN-HG LB/HR % |
| THE CORRECTED GROSS GENERATION IS 575.76 | MWe |
| THE CORRECTED NET GENERATION IS 549.26 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10588.6 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10612.4 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 5829.0 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 650 - 1ST HR

| MEASURED TEST INPUTS FROM FILE wb2hr94a.650 | · |
|--|----------------|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F |
| THE AVERAGE COAL FLOW IS | T.B/HD |
| THE AVERAGE COAL HIGH HEATING VALUE IS | BBL/HR |
| THE AVERAGE OIL HIGH HEATING VALUE IS 0.00 | BTU/BBL |
| | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS | DEG F |
| THE SATURATION PRESSURE FOR THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS | IN-HG LB/HR |
| BACKPRESSURE IS3.71 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | % |
| PRESSURE IS3.27 BPCHG = 0.46 KWCHG = -0.45 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.004531 | % |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10255.3 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10303.7 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 6761.3 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 650 - 2ND HR

| MEASURED TEST INPUTS FROM FILE wb2hr94b.650 | |
|--|--|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| | , |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F |
| TEMPERATURE IS 90.66 THE SATURATION PRESSURE FOR THE AVERAGE MAXIMUM | |
| CONDENSER COOLING WATER TEMPERATURE IS | IN-HG LB/HR |
| BACKPRESSURE IS3.78 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | % |
| PRESSURE IS3.33 BPCHG = 0.47 | % |
| KWCHG = -0.47 THE BACKPRESSURE CORRECTION FACTOR IS | % |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10316.0 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10366.1 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 6720.8 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 750 - 1ST HR

| MEASURED TEST INPUTS FROM FILE wb2hr94a.750 | |
|--|-----------------------|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | |
| CONDENSER IS | DEG F DEG F PCT |
| THE AVERAGE COAL HIGH HEATING VALUE IS | BTU/LB |
| THE AVERAGE OIL HIGH HEATING VALUE IS | BTU/BBL |
| | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | LB/HR |
| BACKPRESSURE IS1.67 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | % |
| PRESSURE IS1.76 BPCHG = -0.09 KWCHG = 0.09 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 0.999070 | % |
| THE CORRECTED GROSS GENERATION IS 785.73 | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10471.6 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10461.5 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 7900.8 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNTI 2 - 750 - 2ND HR

| MEASURED TEST INPUTS FROM FILE wb2hr94b.750 | |
|--|--|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | IN-HG LB/HR |
| BACKPRESSURE IS1.54 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM | % |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS1.54 BPCHG = 0.00 KWCHG = 0.00 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.000000 | 8 |
| THE CORRECTED GROSS GENERATION IS 790.00 | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10428.3 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10428.3 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 7919.3 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNDIT 2 - 840 - 1ST HR

| MEASURED TEST INPUTS FROM FILE wb2hr94a.840 | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWO |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F |
| TEMPERATURE IS | TN-HG |
| BACKPRESSURE IS1.42 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM | % |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS0.74 BPCHG = 0.69 KWCHG = -0.69 | % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.006864 | % |
| THE CORRECTED GROSS GENERATION IS 870.03 | MWe |
| THE CORRECTED NET GENERATION IS 836.53 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10431.8 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10506.3 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 8788.8 | MMBTU |

HEAT RATE CORRECTIONS FOR WHITE BLUFF UNIT 2 - 840 - 2ND HR

| MEASURED TEST INPUTS FROM FILE wb2hr94b.840 | |
|--|---|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F IN-HG LB/HR |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.006383 | ૪ |
| THE CORRECTED GROSS GENERATION IS 876.41 | MWe |
| THE CORRECTED NET GENERATION IS 842.81 | MWe |
| THE UNCORRECTED NET HEAT RATE IS 10273.5 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10341.7 | BTU/NKW |
| THE TOTAL HEAT INPUT IS 8716.0 | MMBTU |

| | REGR | ESSION ANALY | YSIS | | | |
|---|---------------------------------------|--------------------------|---------|-----------|-------------|-------------|
| HEADER DATA FOR | R: E:HR94WB2 | LABEL: | | | | |
| MBER OF CASES | | | LES: 3 | | | |
| | | | | | | |
| TMDEN | | | | | | |
| INDEX NAM 1 CNM 2 CNM DEP. VAR.: HEA | LE: ™ 50 | MEAN 2.4437500 | 233 | STD.DEV. | | |
| 2 CNM | 12^2 30358 | 1.4637500 | 238142. | 5587119 | | |
| DEP. VAR.: HEA | TIN 543 | 0.9975000 | 2221. | 1123272 | | |
| | | | | | | |
| DEPENDENT VARIA | | | | | | |
| VAR. REGRESSI | ON COEFFICIE 7.7103672 .0017835 | NT STD. I | ERROR | T(DF= 13) | PROB. | PARTIAL r^2 |
| CNMW | 7.7103672 | .307 | 73951 | 25.083 | .00000 | .9798 |
| CNM2^2 CONSTANT 10 | 15.5475017 | .000 | 03017 | 5.912 | .00005 | .7289 |
| STD. ERROR OF E | ST. = 52.261 | 8548 | | | | |
| | | | | | | |
| ADJUSTED R SQUA | RED = .99944 RED = .99952 | | | | | |
| | E R = .99976 | | | | | |
| | ANALYSIS | OF VARIANCE | TABLE | | | |
| SOURCE | SUM OF SOUA | PFC DF | MEX | N COUNDE | D DIGTO | 77.07 |
| RESSION 7 | 3964592.6344 | 330 2 3 | 6982296 | .3172170 | 13540.174 | .000E+00 |
| SOURCE FRESSION 7 RESIDUAL TOTAL 7 | 35506.9190 | 687 13 | 2731 | .3014668 | | .0002.00 |
| TOTAL / | 4000099.5535 | 020 15 | | | | |
| OBCEDIED | CAT OUT A MOD | | _ | STANDARDI | ZED RESIDUA | ALS |
| | CALCULATED 2312.675 | | ·2.0 | * | 0 | 2.0 |
| 2 2268.500 | 2279.301 | -10-800602 | | | * | |
| 3 3037.100 | 3021.514 3056.670 3961.695 | 15.586338 | | | * | İ |
| 4 3059.300 5 4048.000 | 3056.670 | 2.630092 | | | * |) |
| 6 3997.900 | 3991.675 | 6.224583 | | | * | * |
| 7 4867.800 | 4907.642 | -39.842243 | | * | ^ | |
| 8 4889.000 | 4862.484 | 26.516310 | | | * | |
| 9 5818.300 | 5859.077 | -40.777168 | | * | | |
| 10 5829.000 11 6761.300 | 5788.588 6843.044 | 40.411519 | | | * | • |
| 12 6720.800 | 6764.254 | -81.743839 -43.453583 | * | * | | |
| 13 7900.800 | 7855.882 | 44.917871 | | ^ | * | |
| 14 7919.300 | 7899.299 | 20.001314 | | | * | |
| 15 8788.800 16 8716.000 | 8713.532 | 75.267809 | | _ | | * |
| 10 0/10.000 | 8778.629 | -62.628557 | , | k | | |

DURBIN-WATSON TEST = 2.2414

White Bluff Plant - Unit One Heat Rate Test Inputs 1995

| Test Load | 160 | 160 | 250 | 250 | 350 | 350 | 450 | 450 | 250 | 550 | 850 | 650 | 750 | 750 | FULL | FULL |
|-----------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| Test Date | 6/21/95 | 6/21/95 | 6/20/95 | 6/20/95 | 6/30/95 | 6/30/95 | 6/20/95 | 6/20/95 | 6/21/95 | 6/21/95 | 6/23/95 | 6/23/95 | 6/30/95 | 6/30/95 | 6/23/95 | 6/23/95 |
| Start Time | 400 | 200 | 400 | 500 | 800 | 900 | 900 | 1000 | 800 | 1000 | 900 | 1000 | 1300 | 1400 | 1400 | 1500 |
| End Time | 200 | 900 | 500 | 900 | 900 | 1000 | 1000 | 1100 | 1000 | 1100 | 1000 | 1100 | 1400 | 1500 | 1500 | 1600 |
| Data File Name | 1160a | 1160b | 1250a | 1250b | 1350a | 1350b | 1450a | 1450b | 1550a | 1550b | 1650a | 1650b | 1750a | 1750b | 1FULLs | 1FULLb |
| Gross Generation (MW) | 190 | 190 | 282 | 280 | 377 | 372 | 481 | 483 | 583 | 586 | 688 | 685 | 781 | 787 | 863 | 863 |
| Aux Usage (MW) | 28.3 | 26.9 | 26.6 | 27.7 | 28.5 | 29.4 | 30.2 | 29.7 | 31.4 | 31 | 33.6 | 34.2 | 36.7 | 36.3 | 38.5 | 37.9 |
| Back Pressure (InHg) | 2.51 | 2.52 | 2.50 | 2.49 | 2.34 | 2.36 | 2.94 | 3.03 | 3.33 | 3,35 | 3.42 | 3.49 | 3.88 | 3.96 | 4,25 | 4.30 |
| Hot Water Temp (DEGF) | 98.86 | 99.69 | 102.05 | 101.55 | 104.54 | 104.73 | 111.73 | 112.98 | 115.91 | 115.93 | 116.01 | 116.74 | 120.15 | 120.91 | 123.22 | 123,53 |
| Cold Water Temp (DEGF) | 90.82 | 90.58 | 90.47 | 90.03 | 91.26 | 91.54 | 95.49 | 96.86 | 97.01 | 97.00 | 94.41 | 95.17 | 95.73 | 96.43 | 96.82 | 90.76 |
| Wet Bulb Temperature (DEGF) | 67.80 | 67.10 | 64.30 | 68.10 | 73.40 | 72.70 | 70.10 | 78.10 | 71.20 | 78.10 | 72.10 | 72.60 | 75.40 | 74.80 | 72.40 | 73.20 |
| Dry Bulb Temperature (DEGF) | 70.20 | 68.70 | 64.70 | 69.60 | 78.30 | 78.50 | 73.00 | 85.00 | 71.80 | 78.90 | 80.40 | 85.60 | 86.30 | 85.60 | 92.00 | 94.00 |
| Coal Flow (PPH) | 269300 | 267200 | 358800 | 363200 | 442200 | 439000 | 582900 | 578700 | 673700 | 671900 | 820400 | 824400 | 902900 | 893900 | 1000800 | 1008000 |
| Coal Heating Value (BTU/#) | 8539.0 | 8643.0 | 8751.0 | 8691.0 | 8763.0 | 8760.0 | 8521.0 | 8565.0 | 8613.0 | 8543.0 | 8449.0 | 8418.0 | 8642.0 | 9695.0 | 8681.0 | 8681.0 |
| Oil Flow (BBL/HR) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Oil Heating Value (BTU/BBL) | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 | 5922000 |

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| | | | _ I | х | Y |
|------|-------|--------|-----|----------|-----------|
| Data | Input | Index: | 1 | 155.3900 | 2299.6000 |
| Data | Input | Index: | 2 | 156.2700 | 2309.4000 |
| Data | Input | Index: | 3 | 245.1700 | 3156.6000 |
| Data | Input | Index: | 4 | 245.6000 | 3139.9000 |
| Data | Input | Index: | 5 | 339.0500 | 3845.6000 |
| Data | Input | Index: | 6 | 344.9300 | 3875.0000 |
| Data | Input | Index: | 7 | 443.6800 | 4966.9000 |
| Data | Input | Index: | 8 | 453.3000 | 4956.6000 |
| Data | Input | Index: | 9 | 544.8400 | 5802.6000 |
| Data | Input | Index: | 10 | 555.0000 | 5740.0000 |
| Data | Input | Index: | 11 | 646.0400 | 6939.8000 |
| Data | Input | Index: | 12 | 649.0200 | 6931.6000 |
| Data | Input | Index: | 13 | 741.6200 | 7802.9000 |
| Data | Input | Index: | 14 | 747.8700 | 7772.5000 |
| Data | Input | Index: | 15 | 808.1600 | 8687.9000 |
| Data | Input | Index: | 16 | 809.7100 | 8750.4000 |

Curve Fit to the Power of 2.

Results:

 $X^2 = 2.73169371315478E-0003$

 $X^1 = 6.98633185603036E+0000$

 $X^0 = 1.19608046828396E+0003$

| MEASURED TEST INPUTS FROM FILE 1160a | |
|--|------------------------------|
| THE AVERAGE GROSS GENERATION IS | 0 MWe 1 IN-HG |
| CONDENSER IS | |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 341000 THE COOLING TOWER RANGE IS. 9.04 THE DESIGN COLD WATER TEMPERATURE IS. 86.54 THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 93.26 THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS. 97.54 THE SATURATION PRESSURE FOR THE AVERAGE MAXIMUM | DEG F DEG F DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | LB/HR |
| BACKPRESSURE IS10.23 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | |
| PRESSURE IS7.03 BPCHG = 3.56 KWCHG = -3.44 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.034360 | 8 |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 14221.1 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

1995 Heat Rate Test Results White Bluff Unit One Page

| MEASURED TEST INPUTS FROM FILE 1160b | |
|---|--------------|
| THE AVERAGE GROSS GENERATION IS | Me IN-HG |
| CONDENSER IS | |
| CONDENSER IS | EG F |
| THE AVERAGE COAL FLOW IS | ם עום |
| THE AVERAGE OIL FLOW IS | BL/HR |
| | ,10,222 |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | EG F |
| THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS | EG F |
| CONDENSER COOLING WATER TEMPERATURE IS | N-HG B/HR |
| BACKPRESSURE IS10.16 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | |
| PRESSURE IS6.69 % BPCHG = 3.87 KWCHG = -3.73 | |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.037267 % | |
| THE CORRECTED GROSS GENERATION IS | we |
| THE CORRECTED NET GENERATION IS | V e |
| THE UNCORRECTED NET HEAT RATE IS 14159.5 BT | ru/nkw |
| THE CORRECTED NET HEAT RATE IS | ru/nkw |
| THE TOTAL HEAT INPUT IS 2309.4 MM | 1BTU |

1995 Heat Rate Test Results

White Bluff Unit One

Page 2

| MEASURED TEST INPUTS FROM FILE 1250a | |
|---|-------------------------|
| THE AVERAGE GROSS GENERATION IS | We N-HG |
| CONDENSER IS | |
| CONDENSER IS | EG F EG F CT S/HR FU/LB |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 341000 GP THE COOLING TOWER RANGE IS. 11.58 DE THE DESIGN COLD WATER TEMPERATURE IS. 84.06 DE THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 93.07 DE THE AVERAGE MAXIMUM CONDENSER COOLING WATER | G F G F G F |
| TEMPERATURE IS | |
| BACKPRESSURE IS8.93 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | |
| PRESSURE IS5.53 % BPCHG = 3.73 KWCHG = -3.60 | |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.035986 % | |
| THE CORRECTED GROSS GENERATION IS 272.20 MWe | e |
| THE CORRECTED NET GENERATION IS 245.60 MWe | e |
| THE UNCORRECTED NET HEAT RATE IS 12293.9 BTU | U/NKW |
| THE CORRECTED NET HEAT RATE IS 12784.2 BTU | U/NKW |
| THE TOTAL HEAT INPUT IS | BTU |

1995 Heat Rate Test Results

White Bluff Unit One

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| MEASURED TEST INPUTS FROM FILE 1250b | |
|---|---|
| THE AVERAGE GROSS GENERATION IS | |
| CONDENSER IS 101.55 DEG F THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE | |
| CONDENSER IS | ` |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 341000 GPM THE COOLING TOWER RANGE IS. 11.52 DEG F THE DESIGN COLD WATER TEMPERATURE IS. 86.68 DEG F THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 93.26 DEG F THE AVERAGE MAXIMUM CONDENSER COOLING WATER | |
| TEMPERATURE IS | |
| CONDENSER COOLING WATER TEMPERATURE IS | |
| BACKPRESSURE IS9.01 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | |
| PRESSURE IS | |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.026116 % | |
| THE CORRECTED GROSS GENERATION IS 272.87 MWe | |
| THE CORRECTED NET GENERATION IS 245.17 MWe | |
| THE UNCORRECTED NET HEAT RATE IS 12511.2 BTU/NKV | |
| THE CORRECTED NET HEAT RATE IS 12874.8 BTU/NKW | V |
| THE TOTAL HEAT INPUT IS | |

| | White Pluff II-16 C | |
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| 1995 Heat Rate Test Results | | |
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| | White Bluff Unit One | |
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| | Writte Bluff Unit One | |
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| М | EASURED TEST INPUTS FROM FILE 1350a | |
|------------------|---|------------------------------|
| T T | THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| T | ONDENSER IS | |
| T T T T | ONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| C. | ALCULATED RESULTS | |
| TI TI TI | HE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F |
| TI TI | EMPERATURE IS | |
| TF | ONDENSER COOLING WATER TEMPERATURE IS | LB/HR |
| CC | ACKPRESSURE IS8.28 HE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM ONDENSER COOLING WATER TEMPERATURE SATURATION | |
| PF BF | RESSURE IS7.39 PCHG = 0.97 ICHG = -0.96 | ક |
| TH | E BACKPRESSURE CORRECTION FACTOR IS 1.009565 | 8 |
| TH | E CORRECTED GROSS GENERATION IS | MWe |
| TH | E CORRECTED NET GENERATION IS | MWe |
| TH | E UNCORRECTED NET HEAT RATE IS | BTU/NKW |
| TH | E CORRECTED NET HEAT RATE IS | BTU/NKW |
| TH | E TOTAL HEAT INPUT IS | MMBTU |

1995 Heat Rate Test Results

White Bluff Unit One

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| MEASURED TEST INPUTS FROM FILE 1350b | |
|---|---|
| THE AVERAGE GROSS GENERATION IS | |
| CONDENSER IS | |
| CONDENSER IS | |
| CALCULATED RESULTS | _ |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 341000 GPM THE COOLING TOWER RANGE IS. 13.19 DEG F THE DESIGN COLD WATER TEMPERATURE IS. 90.73 DEG F THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 93.99 DEG F THE AVERAGE MAXIMUM CONDENSER COOLING WATER | |
| TEMPERATURE IS | |
| CONDENSER COOLING WATER TEMPERATURE IS | |
| BACKPRESSURE IS8.27 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | |
| PRESSURE IS | |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.009635 % | |
| THE CORRECTED GROSS GENERATION IS 368.45 MWe | |
| THE CORRECTED NET GENERATION IS | |
| THE UNCORRECTED NET HEAT RATE IS 11224.9 BTU/NKW | |
| THE CORRECTED NET HEAT RATE IS | |
| THE TOTAL HEAT INPUT IS | |

1995 Heat Rate Test Results White Bluff Unit One Page 6

| MEASURED TEST INPUTS FROM FILE 1450a |
|---|
| THE AVERAGE GROSS GENERATION IS |
| CONDENSER IS |
| CONDENSER IS |
| CALCULATED RESULTS |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 341000 GPM THE COOLING TOWER RANGE IS. 16.24 DEG F THE DESIGN COLD WATER TEMPERATURE IS. 88.55 DEG F THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 93.78 DEG F THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS. 100.34 DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS |
| BACKPRESSURE IS4.96 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION |
| PRESSURE IS3.51 % BPCHG = 1.53 KWCHG = -1.50 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.015024 % |
| THE CORRECTED GROSS GENERATION IS 473.88 MWe |
| THE CORRECTED NET GENERATION IS |
| THE UNCORRECTED NET HEAT RATE IS |
| THE CORRECTED NET HEAT RATE IS |
| THE TOTAL HEAT INPUT IS |

| 1995 Heat Pate Test Results | |
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| 1995 Heat Rate Test Results White Bluff Unit One | |
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| 1995 Heat Rate Test Results White Bluff Unit One | |
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| Willie Bluit Only One | Page 7 |
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| MEASURED TEST INPUTS FROM FILE 1450b | |
|--|---|
| THE AVERAGE GROSS GENERATION IS | 70 MWe 03 IN-HG |
| CONDENSER IS | 10 DEG F |
| CONDENSER IS | LO DEG F DO DEG F LS PCT DO LB/HR DO BTU/LB DO BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 34100 THE COOLING TOWER RANGE IS. 16.1 THE DESIGN COLD WATER TEMPERATURE IS. 94.2 THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 94.2 THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS. 96.2 THE SATURATION PRESSURE FOR THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS. 3.0 | 2 DEG F 8 DEG F 8 DEG F 8 DEG F |
| THE TURBINE THROTTLE FLOW IS | 0 LB/HR |
| BACKPRESSURE IS4.6 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | 6 % |
| PRESSURE IS4.6 BPCHG = 0.00 KWCHG = 0.00 | 6 % |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.00000 | 0 % |
| THE CORRECTED GROSS GENERATION IS | 0 MWe |
| THE CORRECTED NET GENERATION IS 453.3 | 0 MWe |
| THE UNCORRECTED NET HEAT RATE IS | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

1995 Heat Rate Test Results White Bluff Unit One Page 8

| MEASURED TEST INPUTS FROM FILE 1550a |
|--|
| THE AVERAGE GROSS GENERATION IS |
| CONDENSER IS |
| CONDENSER IS |
| CALCULATED RESULTS |
| THE COOLING TOWER CIRCULATING WATER FLOW IS |
| TEMPERATURE IS |
| BACKPRESSURE IS3.12 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS1.97 % BPCHG = 1.19 KWCHG = -1.17 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.011726 % |
| THE CORRECTED GROSS GENERATION IS |
| THE CORRECTED NET GENERATION IS 544.84 MWe |
| THE UNCORRECTED NET HEAT RATE IS 10519.5 BTU/NKW |
| THE CORRECTED NET HEAT RATE IS |
| THE TOTAL HEAT INPUT IS |

| 1995 Heat Rate Test Results | | |
|-----------------------------|------------------|---------------|
| | White Bluff Unit | |
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| | | ricone Page 9 |
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| MEASURED TEST INPUTS FROM FILE 1550b | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 341000 (THE COOLING TOWER RANGE IS. 18.93 I THE DESIGN COLD WATER TEMPERATURE IS. 93.57 I THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 93.57 I THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS. 97.00 I THE SATURATION PRESSURE FOR THE AVERAGE MAXIMUM | DEG F DEG F DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | LB/HR |
| BACKPRESSURE IS3.05 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | |
| PRESSURE IS | B |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.000000 % | \$ |
| THE CORRECTED GROSS GENERATION IS 586.00 M | W e |
| THE CORRECTED NET GENERATION IS 555.00 M | I We |
| THE UNCORRECTED NET HEAT RATE IS 10342.4 B | TU/NKW |
| THE CORRECTED NET HEAT RATE IS 10342.4 B | TU/NKW |
| THE TOTAL HEAT INPUT IS 5740.0 M | MBTU |

1995 Heat Rate Test Results White Bluff Unit One Page 10

| MEASURED TEST INPUTS FROM FILE 1650a | |
|--|-----------------------|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT |
| THE AVERAGE COAL HIGH HEATING VALUE IS 8449.00 | BTU/LB BBL/HR |
| | BTU/BBL |
| | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEC E |
| THE DESIGN COLD WATER TEMPERATURE IS | DEG E |
| THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS | DEG F |
| THE SATURATION PRESSURE FOR THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS | LB/HR |
| BACKPRESSURE IS2.36 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | * |
| PRESSURE IS1.58 BPCHG = 0.80 KWCHG = -0.79 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.007889 | 8 |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 10680.1 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

| 995 Heat Rate Test Results | | |
|----------------------------|----------------------|---------|
| | White Bluff Unit One | |
| | | |
| | | Page 11 |
| | | |
| | | |

| MEASURED TEST INPUTS FROM FILE 1650b | |
|---|--------------------|
| THE AVERAGE GROSS GENERATION IS | |
| CONDENSER IS 116.74 DEG THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE | |
| CONDENSER IS | F F IR LB |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 341000 GPM THE COOLING TOWER RANGE IS. 21.57 DEG THE DESIGN COLD WATER TEMPERATURE IS. 92.70 DEG THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 95.89 DEG THE AVERAGE MAXIMUM CONDENSER COOLING WATER | F F |
| TEMPERATURE IS | |
| CONDENSER COOLING WATER TEMPERATURE IS | G R |
| BACKPRESSURE IS2.23 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | |
| PRESSURE IS1.54 % BPCHG = 0.71 KWCHG = -0.70 | |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.007003 % | |
| THE CORRECTED GROSS GENERATION IS 680.24 MWe | |
| THE CORRECTED NET GENERATION IS 646.04 MWe | |
| THE UNCORRECTED NET HEAT RATE IS 10663.5 BTU/N | IKW |
| THE CORRECTED NET HEAT RATE IS 10742.1 BTU/N | IKW |
| THE TOTAL HEAT INPUT IS | ī |

1995 Heat Rate Test Results White Bluff Unit One Page 12

| MEASURED TEST INPUTS FROM FILE 1750a |
|---|
| THE AVERAGE GROSS GENERATION IS |
| CONDENSER IS |
| CONDENSER IS |
| CALCULATED RESULTS |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 341000 GPM THE COOLING TOWER RANGE IS. 24.42 DEG F THE DESIGN COLD WATER TEMPERATURE IS. 93.70 DEG F THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 95.61 DEG F THE AVERAGE MAXIMUM CONDENSER COOLING WATER |
| TEMPERATURE IS 97.63 DEG F THE SATURATION PRESSURE FOR THE AVERAGE MAXIMUM |
| CONDENSER COOLING WATER TEMPERATURE IS |
| BACKPRESSURE IS1.11 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION |
| PRESSURE IS0.77 % BPCHG = 0.35 KWCHG = -0.34 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.003445 % |
| THE CORRECTED GROSS GENERATION IS |
| THE CORRECTED NET GENERATION IS |
| THE UNCORRECTED NET HEAT RATE IS |
| THE CORRECTED NET HEAT RATE IS |
| THE TOTAL HEAT INPUT IS 7802.9 MMBTU |

| | White Bluff Unit One | |
|---------------------------|----------------------|---------|
| | | |
| 95 Heat Rate Test Results | | |
| | White Bluff Unit One | |
| | | |
| | | |
| | | Page 13 |
| | | |
| | | |
| | White Blum Unit One | |

| MEACURED EDGE TAXBURG TO A TO |
|--|
| MEASURED TEST INPUTS FROM FILE 1750b |
| THE AVERAGE GROSS GENERATION IS |
| CONDENSER IS |
| CONDENSER IS |
| CALCULATED RESULTS |
| THE COOLING TOWER CIRCULATING WATER FLOW IS |
| TEMPERATURE IS |
| BACKPRESSURE IS0.96 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION |
| PRESSURE IS0.60 % BPCHG = 0.36 KWCHG = -0.36 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.003612 % |
| THE CORRECTED GROSS GENERATION IS |
| THE CORRECTED NET GENERATION IS 747.87 MWe |
| THE UNCORRECTED NET HEAT RATE IS 10353.6 BTU/NKW |
| THE CORRECTED NET HEAT RATE IS |
| THE TOTAL HEAT INPUT IS |

1995 Heat Rate Test Results

White Bluff Unit One

Page 14

Claim Withdrawn. Contains No CBI. 06/29/2016_YD

| MEASURED TEST INPUTS FROM FILE 1fulla |
|--|
| THE AVERAGE GROSS GENERATION IS |
| CONDENSER IS 123.22 DEG F THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE |
| CONDENSER IS |
| CALCULATED RESULTS |
| THE COOLING TOWER CIRCULATING WATER FLOW IS |
| TEMPERATURE IS |
| CONDENSER COOLING WATER TEMPERATURE IS |
| BACKPRESSURE IS0.39 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION |
| PRESSURE IS |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.007486 % |
| THE CORRECTED GROSS GENERATION IS 846.66 MWe |
| THE CORRECTED NET GENERATION IS 808.16 MWe |
| THE UNCORRECTED NET HEAT RATE IS 10666.6 BTU/NKW |
| THE CORRECTED NET HEAT RATE IS |
| THE TOTAL HEAT INPUT IS 8687.9 MMBTU |

1995 Heat Rate Test Results White Bluff Unit One Page 15

| MEASURED TEST INPUTS FROM FILE 1fullb |
|---|
| THE AVERAGE GROSS GENERATION IS |
| CONDENSER IS |
| CONDENSER IS |
| CALCULATED RESULTS |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 341000 GPM THE COOLING TOWER RANGE IS. 26.47 DEG F THE DESIGN COLD WATER TEMPERATURE IS. 95.04 DEG F THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 98.42 DEG F THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS. 100.45 DEG F THE SATURATION PRESSURE FOR THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS. 4.70 IN-HG THE TURBINE THROTTLE FLOW IS. 5818548.00 LB/HR THE HEAT RATE CORRECTION FACTOR FOR CONDENSER BACKPRESSURE IS. -0.31 % |
| CONDENSER COOLING WATER TEMPERATURE SATURATION |
| PRESSURE IS |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.006361 % |
| THE CORRECTED GROSS GENERATION IS 847.61 MWe |
| THE CORRECTED NET GENERATION IS 809.71 MWe |
| THE UNCORRECTED NET HEAT RATE IS |
| THE CORRECTED NET HEAT RATE IS 10806.9 BTU/NKW |
| THE TOTAL HEAT INPUT IS 8750.4 MMBTU |

1995 Heat Rate Test Results

White Bluff Unit One

Page 16



Inter-Office Correspondence

Date:

July 18, 1995

To:

Mr. Jim Campbell T-EP-16
Mr. Mike Bakewell T-EP-16
Mr. Lynn Sanders A-WB
Mr. William Phillips A-SOC

Mr. William Phillips
Mr. Henry Thompson

A-TCBY-23G

From:

Pat Klepper

Phone: 8-762-4529

Roger Lawson

Phone: 8-764-7329

Subject:

1995 White Bluff Plant - Heat Rate Test Results

Heat rate tests were performed on both White Bluff Units from June 20 through June 30. Co-owners were notified prior to the tests and representatives of Arkansas Electric Co-operative were present to observe the testing. Testing was performed in an unbiased manner per Entergy procedure dated November 30, 1992. The Unit 2 load range was restricted due to air preheater flow restrictions.

Our calculations, analysis, and review are now complete and the results are attached for your reference. It is our recommendation that the results be implemented for dispatch and co-owner billing. The new coefficients for the heat rate equations are;

| - | ~ | • . | \sim | |
|---|---|-----|--------|-----|
| | 111 | 1 | O: | ne |
| | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | | • | 110 |

X² = 2.73169371315478E-0003 X¹ = 6.98633185603036E+0000 X⁰ = 1.19608046828396E+0003

Unit Two

 X^2 = 1.32874423471649E-0003 X^1 = 8.42371123335924E+0000 X^0 = 9.53025351923540E+0002

If you need any additional information, please do not hesitate to contact either Roger Lawson or Pat Klepper.

τ 10/03/95 08:55 **23**501 698 4512 IND. PLANT →→→ PLANT SUPPORT **2**003/020

Pat Klepper

WPK/wpk

w/Attachments

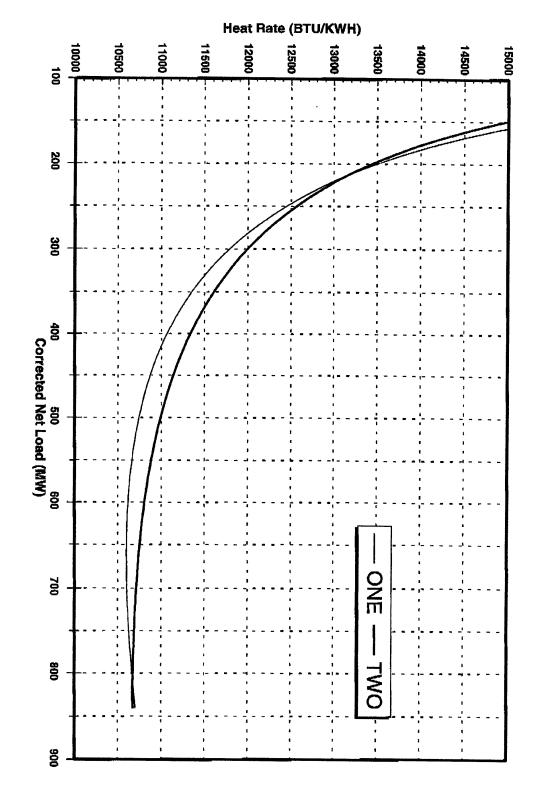
C: George Eubanks

A-WB-SC Phil Carter A-SOC Robert Rickett A-WB

David Harris A.E.C.C.



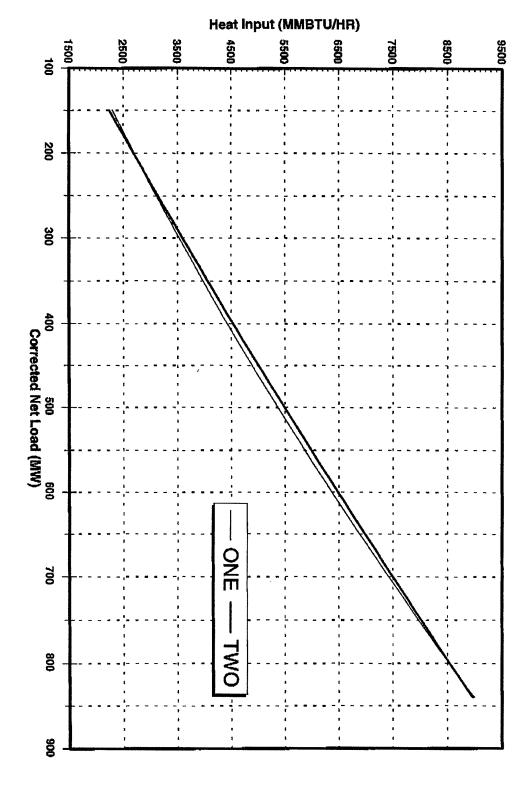
White Bluff Plant 1995 Heat Rate Test Results



07/18/95

10/03/95 08:55 \$201 698 4512 IND. PLANT \$\delta \text{TVPOFT} \qquad \text{\$\omega\$} \text{\$\omega\$} \qquad \qquad \text{\$\omega\$} \qquad \qqqq \qqq \qqqq \qqq \qqqq \qqqq \qqq \qqqq \qqqq \qqq \qqq \qqqq \qqq


White Bluff Plant 1995 Heat Rate Test Results



07/18/85

070/10000

→→→ PLANT SUPPORT

IND. PLANT

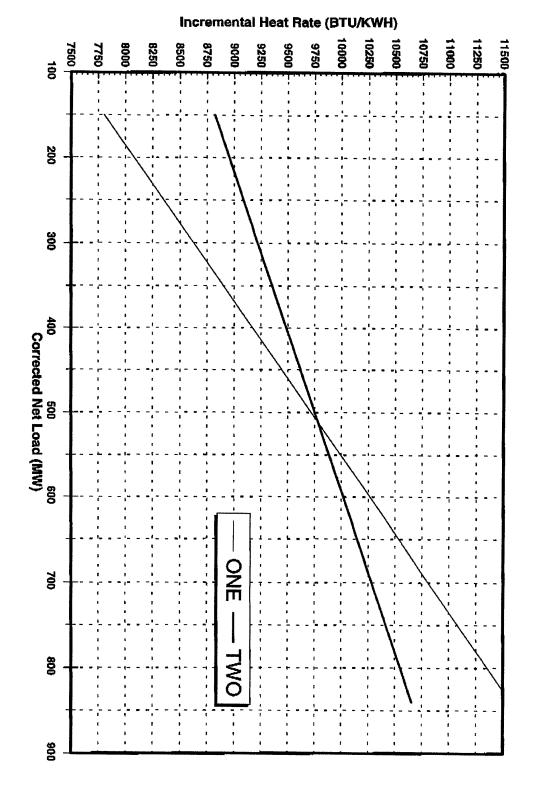
₩207 888 4215

99:80

T0/03/82 C



White Bluff Plant 1995 Heat Rate Test Results



07/18/95

070/9002

→→→ PLANT SUPPORT

IND. PLANT

2201 888 4215

08:22

96/00/0T

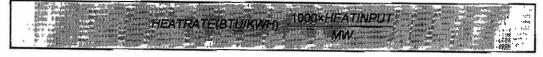
White Bluff Plant - Unit One **Heat Rate Test Results** 1995

| CORRECTED | HEAT |
|-----------|-----------|
| net | INPUT |
| MW | MMBTU/HR |
| 155.3900 | 2299.6000 |
| 156.2700 | 2309.4000 |
| 245.1700 | 3156.6000 |
| 245.6000 | 3139.9000 |
| 339.0500 | 3845.6000 |
| 344.9300 | 3875.0000 |
| 443.6800 | 4966.9000 |
| 453.3000 | 4956.6000 |
| 544.8400 | 5802.6000 |
| 555.0000 | 5740.0000 |
| 646.0400 | 6939.8000 |
| 649.0200 | 6931.6000 |
| 741.6200 | 7802.9000 |
| 747.8700 | 7772.5000 |
| 808.1600 | 8687.9000 |
| 809.7100 | 8750.4000 |
| | |

HEAT INPUT EQUATION



HEAT RATE EQUATION

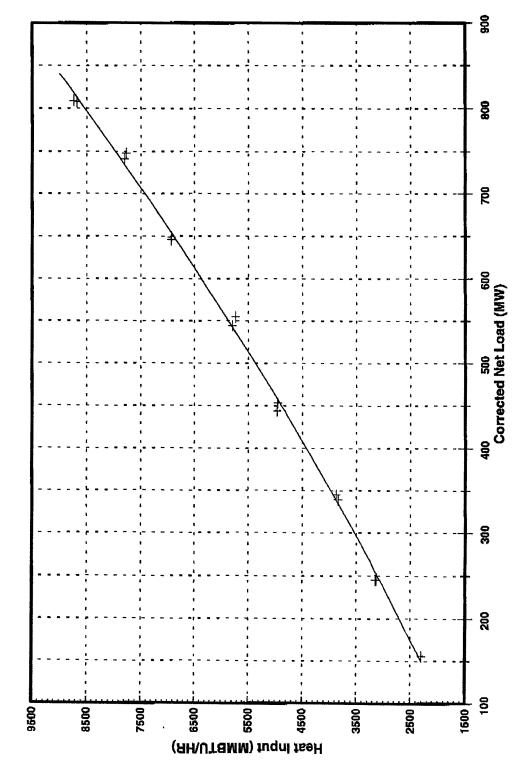


INCREMENTAL HEAT RATE EQUATION

INCREMENTALHEATRATE(BTUIKWH) = [6.986332 + 0.0054634 × MW] × 1000



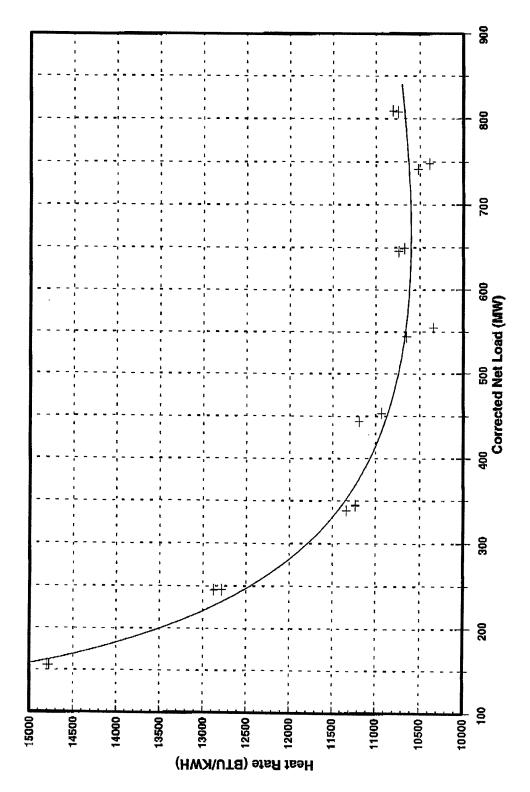
White Bluff Unit One 1995 Heat Rate Test Results



Claim Withdrawn. Contains No CBI. 06/29/2016_YD

H:WRIWB\1995\WB1

White Bluff Unit One 1995 Heat Rate Test Results

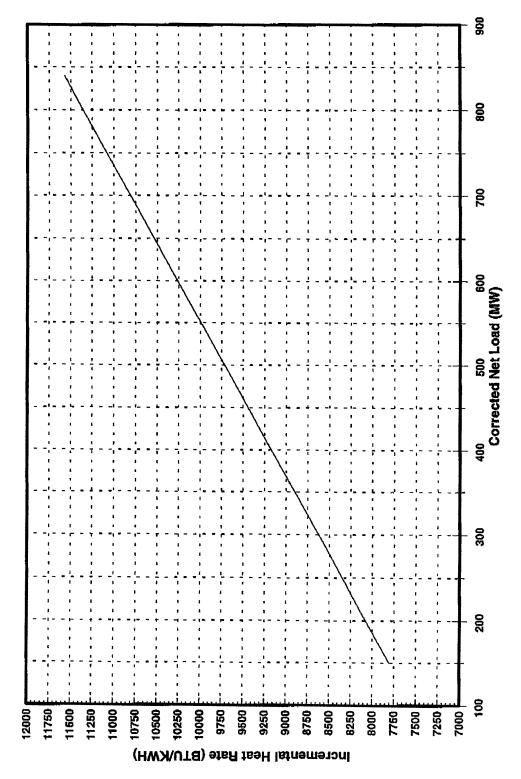


Claim Withdrawn. Contains No CBI. 06/29/2016_YD

H:\HF\WB\1995\HR1995.WB1



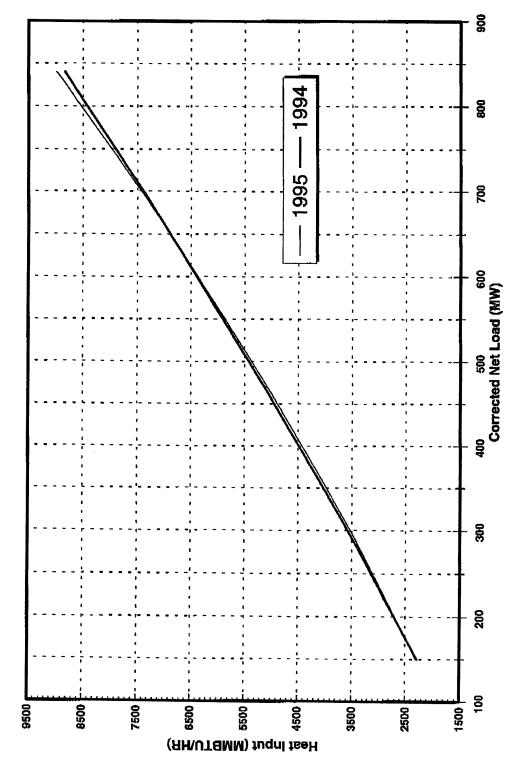
1995 Heat Rate Test Results White Bluff Unit One



Claim Withdrawn. Contains No CBI. 06/29/2016_YD

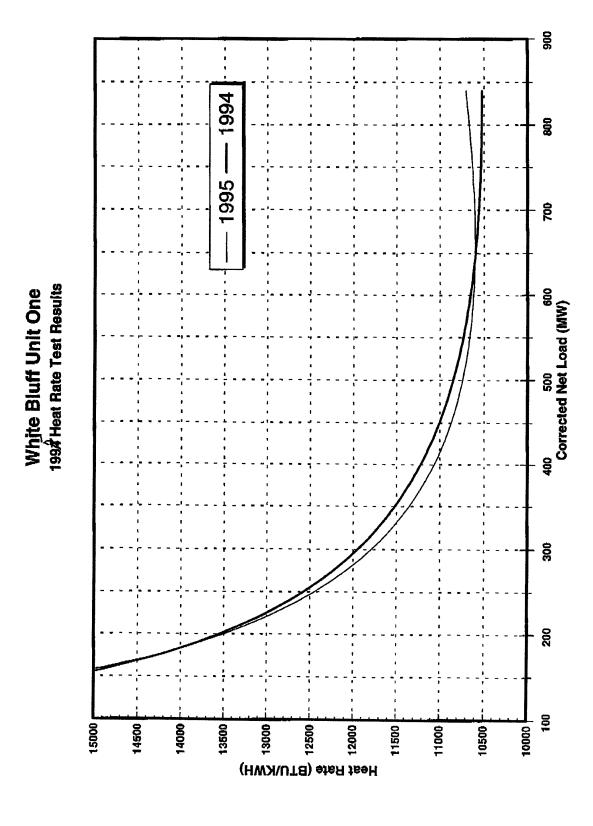
H:WEWBY1995WR1995.WB1





Claim Withdrawn. Contains No CBI. 06/29/2016_YD

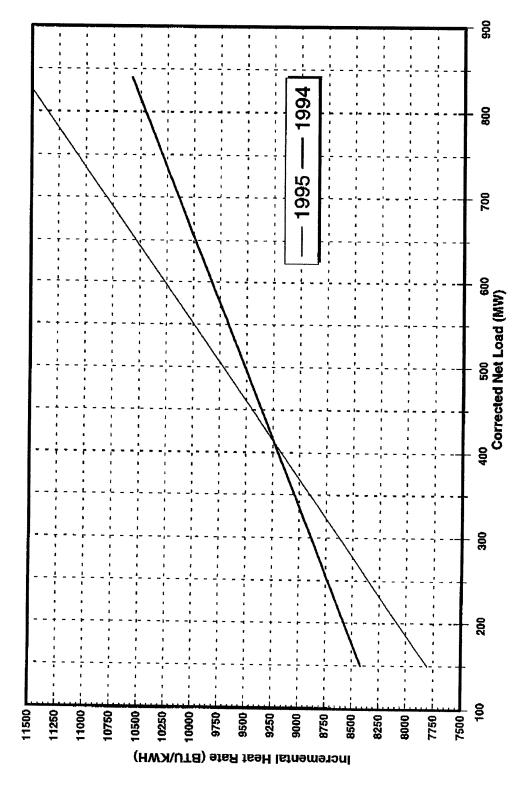
H:\HR\WB\1995\HR\1995\WB1



HAHRIWB(1995)HR1995.WB1

Claim Withdrawn. Contains No CBI. 06/29/2016_YD

White Bluff Unit One 1994 Heat Rate Test Results



Claim Withdrawn. Contains No CBI. 06/29/2016_YD

HURIWEN1995/HR1995,WB1

→→→ PLANT SUPPORT

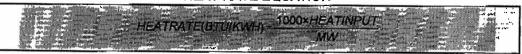
White Bluff Plant - Unit Two **Heat Rate Test Results** 1995

| CORRECTED | HEAT |
|-----------|-----------|
| net | INPUT |
| WM | MMBTU/HR |
| 157.9900 | 2330.5000 |
| 160.6000 | 2299.8000 |
| 235.2000 | 3044.8000 |
| 236.1900 | 3016.8000 |
| 315.1100 | 3729.4000 |
| 316.6100 | 3726.1000 |
| 382.0200 | 4401.2000 |
| 385.7700 | 4399.1000 |
| 464.1100 | 5223.8000 |
| 467.8000 | 5183.7000 |
| 552.5000 | 5977.2000 |
| 553.6000 | 5951.4000 |
| 626.2300 | 6753.1000 |
| 631.8600 | 6778.6000 |
| 695.7500 | 7525.3000 |
| 697.6000 | 7456-9000 |

HEAT INPUT EQUATION

HEATINPUT(MMBTUIHR) = 953.025352 +8.423711×MW+0.001328744×MV

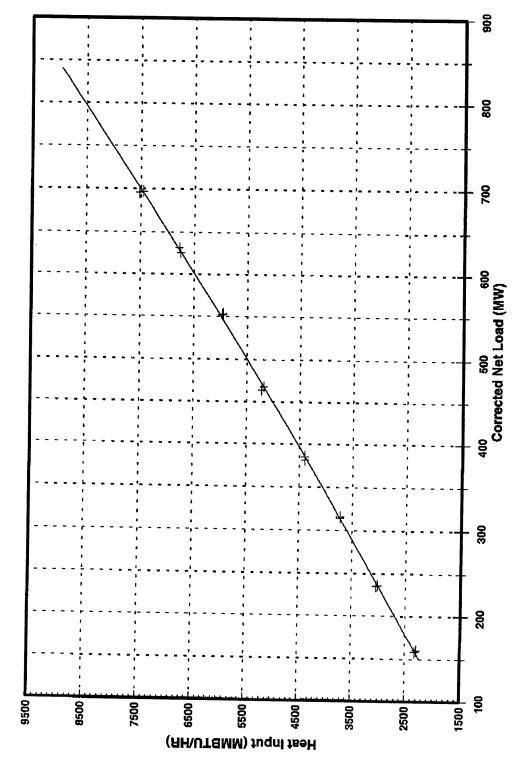
HEAT RATE EQUATION



INCREMENTAL HEAT RATE EQUATION

INCREMENTALHEATRATE(BTUIKWH) = 18.423711 + 0.0026575*MW]*1000

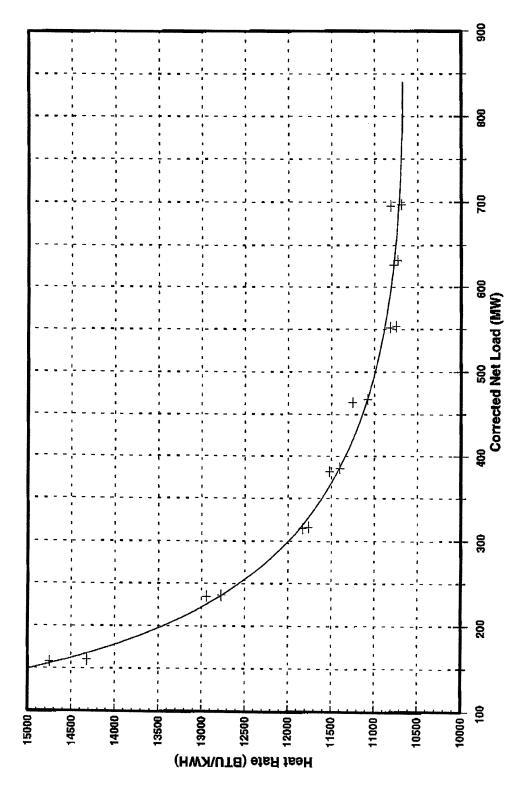
White Bluff Unit Two 1995 Heat Rate Test Results



Claim Withdrawn. Contains No CBI. 06/29/2016_YD

H:WR\WB\1995WR1995.WB1

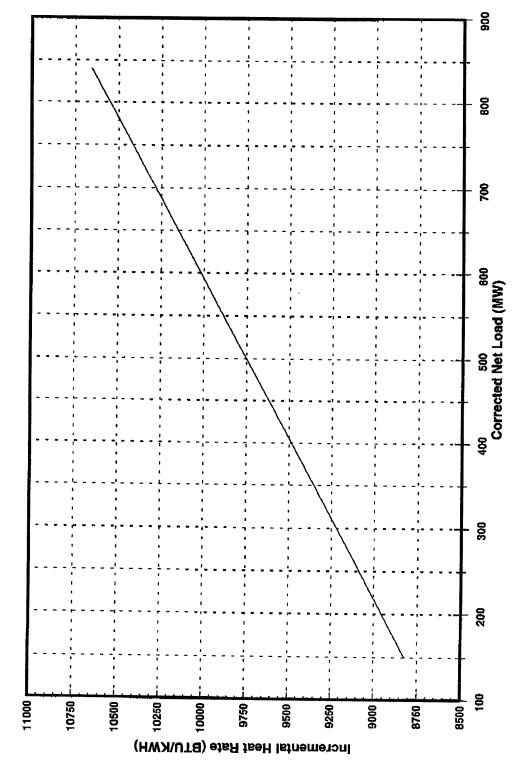
White Bluff Unit Two 1995 Heat Rate Test Results



Claim Withdrawn. Contains No CBI. 06/29/2016_YD

H:MRIWB(1995)HR1996,WB1

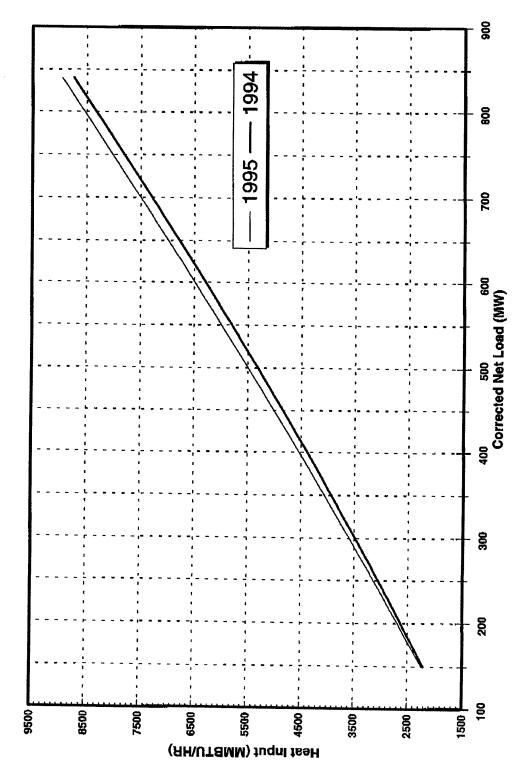
White Bluff Unit Two 1995 Heat Rate Test Results



Claim Withdrawn. Contains No CBI. 06/29/2016_YD

H:HRWEN1995NR1995.WB1

White Bluff Unit Two 1995 Heat Rate Test Results



Claim Withdrawn. Contains No CBI. 06/29/2016_YD

HAMMEN 1985 VIRT 1895 WET

07/18/95

900 1994 800 1995 700 1995 Heat Rate Test Results White Bluff Unit Two 400 500 600 Corrected Net Load (MW) 300 200 5 15000 14500 14000 13500 13000 12500 11500 11000 10500 10000 Heat Rate (BTU/KWH)

Claim Withdrawn. Contains No CBI. 06/29/2016_YD

H:UHRIWB\1995\HR1995.WB1

White Bluff Unit Two 1995 Heat Rate Test Results 0 500 600 Corrected Net Load (MW) Incremental Heat Rate (BTU/KWH)

Claim Withdrawn. Contains No CBI. 06/29/2016_YD

HAHRIWEN 1995 HR 1985. WB 1

White Bluff Plant - Unit Two Heat Rate Test Inputs 1995

| Test Load | 160 | 160 | 240 | 240 | 316 | 315 | 385 | 395 | 470 | 470 | 550 | 250 | 630 | 630 | 700 | 700 |
|-----------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| Test Date | 6/26/95 | 6/26/95 | 6/27/95 | 6/27/95 | 6/28/95 | 6/28/95 | 6/26/95 | 6/26/95 | 6/27/95 | 6/27/95 | 6/29/95 | 6/29/95 | 6/28/95 | 6/28/95 | 6/29/95 | 6/29/95 |
| Start Time | 400 | 200 | 400 | 200 | 900 | 1000 | 006 | 1000 | 006 | 1000 | 1000 | 1100 | 1400 | 1500 | 1500 | 1600 |
| End Time | 200 | 900 | 200 | 900 | 1000 | 1100 | 1000 | 1100 | 1000 | 1100 | 1100 | 1200 | 1500 | 1600 | 1600 | 1700 |
| Data File Name | 2160a | 2160b | 2240a | 2240b | 2315a | 2315b | 2395a | 2395b | 2470a | 2470b | 2550a | 2550b | 2630a | 2630b | 2FULLa | 2FULLb |
| Gross Generation (MW) | 188 | 191 | 268 | 569 | 345 | 343 | 419 | 416 | 503 | 200 | 581 | 582 | 629 | 999 | 735 | 732 |
| Aux Usage (MW) | 23.1 | 22.5 | 23.5 | 23.5 | 23.7 | 23.7 | 25 | 25.2 | 26.4 | 26.4 | 28.5 | 28.4 | 29.9 | 30 | 32.3 | 32.1 |
| Back Pressure (InHg) | 1.600 | 1.600 | 1.750 | 1,750 | 2.240 | 2,290 | 2.430 | 2.520 | 2.720 | 2.780 | 3.600 | 3.620 | 3.800 | 3.910 | 4.000 | 3,980 |
| Hot Water Temp (DEGF) | 89.64 | 89.10 | 93,95 | 94.28 | 102.21 | 103.01 | 104.45 | 105.61 | 106.99 | 108.50 | 117.11 | 117.40 | 118.88 | 119.80 | 119.89 | 119.88 |
| Cold Water Temp (DEGF) | 81.98 | 81.33 | 83.82 | 84.08 | 89.38 | 90.16 | 89.57 | 90.69 | 89.47 | 90.87 | 96.81 | 97.11 | 95.94 | 96.73 | 94.61 | 94.71 |
| Wet Bulb Temperature (DEGF) | 64.10 | 62.80 | 62.40 | 61.80 | 70.50 | 71.80 | 66.70 | 67.00 | 66.50 | 67.30 | 77.50 | 78.40 | 75.10 | 75.40 | 72.50 | 74.10 |
| Dry Bulb Temperature (DEGF) | 68.00 | 66.10 | 68.50 | 66.00 | 78.50 | 81.00 | 77.30 | 81.00 | 77.60 | 81.70 | 91.00 | 93.80 | 87.30 | 87.70 | 76,50 | 78.40 |
| Coal Flow (PPH) | 266500 | 265900 | 352900 | 351400 | 427600 | 432700 | 515300 | 514700 | 603600 | 908900 | 694700 | 691700 | 787900 | 786200 | 858200 | 857000 |
| Coal Heating Value (BTU/#) | 8745.0 | 8649.0 | 8628.0 | 8585.0 | 8714.0 | 8619.0 | 8537.0 | 8551.0 | 8588.0 | 8579.0 | 8604.0 | 8604.0 | 8571.0 | 8622.0 | 8689.0 | 8781.0 |
| Oll Flow (BBL/HR) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ٥ |
| Oil Heating Value (BTU/BBL) | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 | 5748106 |

Claim Withdrawn. Contains No CBI. 06/29/2016_YD

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| ****** | | | _ I | х | Y |
|--------|-------|--------|-----|----------|-----------|
| Data | Input | Index: | 1 | 157.9900 | 2330.5000 |
| Data | Input | Index: | 2 | 160.6000 | 2299.8000 |
| Data | Input | Index: | 3 | 235.2000 | 3044.8000 |
| Data | Input | Index: | 4 | 236.1900 | 3016.8000 |
| Data | Input | Index: | 5 | 315.1100 | 3729.4000 |
| Data | Input | Index: | 6 | 316.6100 | 3726.1000 |
| Data | Input | Index: | 7 | 382.0200 | 4401.2000 |
| Data | Input | Index: | 8 | 385.7700 | 4399.1000 |
| Data | Input | Index: | 9 | 464.1100 | 5223.8000 |
| Data | Input | Index: | 10 | 467.8000 | 5183.7000 |
| Data | Input | Index: | 11 | 552.5000 | 5977.2000 |
| Data | Input | Index: | 12 | 553.6000 | 5951.4000 |
| Data | Input | Index: | 13 | 626.2300 | 6753.1000 |
| Data | Input | Index: | 14 | 631.8600 | 6778.6000 |
| Data | Input | Index: | 15 | 695.7500 | 7525.3000 |
| Data | Input | Index: | 16 | 697.6000 | 7456.9000 |

Curve Fit to the Power of 2.

Results:

 $X^2 = 1.32874423471649E-0003$

 $X^1 = 8.42371123335924E+0000$

 $X^0 = 9.53025351923540E+0002$

| MEASURED TEST INPUTS FROM FILE 2160a | |
|---|---------|
| THE AVERAGE GROSS GENERATION IS |) MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F |
| THE COMPUTED RELATIVE HUMIDITY IS | LR/HR |
| | BTU/BBL |
| | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS | |
| CONDENSER COOLING WATER TEMPERATURE IS | LB/HR |
| BACKPRESSURE IS16.74 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | 8 |
| PRESSURE IS13.44 BPCHG = 3.97 KWCHG = -3.82 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS | 8 |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS | BTU/NKW |
| THE TOTAL HEAT INPUT IS 2330.5 | MMBTU |

1995 Heat Rate Test Results

White Bluff Unit Two

Page 1

| MEASURED TEST INPUTS FROM FILE 2160b | |
|--|-----------------|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 341000 THE COOLING TOWER RANGE IS. 7.77 THE DESIGN COLD WATER TEMPERATURE IS. 83.35 THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 93.37 THE AVERAGE MAXIMUM CONDENSER COOLING WATER | DEG F |
| TEMPERATURE IS | TN-HG |
| THE TURBINE THROTTLE FLOW IS | LB/HR |
| BACKPRESSURE IS16.63 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | ક |
| PRESSURE IS12.87 BPCHG = 4.51 KWCHG = -4.31 | ક |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.043140 | 8 |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS | BTU/NKW |
| THE TOTAL HEAT INPUT IS 2299.8 | MMBTU |

1995 Heat Rate Test Results

White Bluff Unit Two

Page 2

Claim Withdrawn. Contains No CBI. 06/29/2016_YD

| MEASURED TEST INPUTS FROM FILE 2240a | |
|--|-------------------------------------|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULAMED DEGITES | |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | GPM DEG E |
| THE DESIGN COLD WATER TEMPERATURE IS | DEG F |
| THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS 94.10 THE AVERAGE MAXIMUM CONDENSER COOLING WATER | DEG F |
| TEMPERATURE IS | DEG F |
| CONDENSER COOLING WATER TEMPERATURE IS | TN-HC |
| THE TURBINE THROTTLE FLOW IS | LB/HR |
| BACKPRESSURE IS13.19 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM | 8 |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS9.95 BPCHG = 3.73 | 8 |
| KWCHG = -3.60 THE BACKPRESSURE CORRECTION FACTOR IS 1.035961 | 8 |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 12453.3 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

1995 Heat Rate Test Results

White Bluff Unit Two

Page 3

| MEASURED TEST INPUTS FROM FILE 2240b | |
|--|-------------------------------------|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F |
| THE HEAT RATE CORRECTION FACTOR FOR CONDENSER BACKPRESSURE IS13.16 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | 8 |
| PRESSURE IS9.93 BPCHG = 3.72 KWCHG = -3.59 | |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.035860 | |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 12288.3 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS 12772.8 | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

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| 1995 Heat Rate Test Results | | |
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Claim Withdrawn. Contains No CBI. 06/29/2016_YD

| MEASURED TEST INPUTS FROM FILE 2315a | |
|--|-----------------------|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| TEMPERATURE IS | |
| THE TURBINE THROTTLE FLOW IS | LB/HR |
| BACKPRESSURE IS9.22 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | ક |
| PRESSURE IS7.95 BPCHG = 1.40 KWCHG = -1.38 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS | ४ |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

1995 Heat Rate Test Results

White Bluff Unit Two

Page 5

| MEASURED TEST INPUTS FROM FILE 2315b | |
|---|--|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F DEG F IN-HG LB/HR |
| KWCHG = -1.24 THE BACKPRESSURE CORRECTION FACTOR IS 1.012356 | 8 |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

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| 1995 Heat Rate Test Res | sults White Bluff Unit Two | Dogo 6 |
| | Willie Orall Olik TWO | Page 6 |
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| MEAS | SURED TEST INPUTS FROM FILE 2395a | |
|---|---|--|
| THE THE THE | AVERAGE GROSS GENERATION IS | MWe IN-HG |
| THE | DENSER IS | |
| CONI THE THE THE THE THE | DENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALC | CULATED RESULTS | |
| THE THE THE TEMP THE COND THE BACK THE COND | COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F DEG F IN-HG LB/HR |
| BPCH KWCH | SURE IS5.41 IG = 2.05 IG = -2.00 | |
| | BACKPRESSURE CORRECTION FACTOR IS | |
| | CORRECTED GROSS GENERATION IS | |
| | INCODECUED NEW HEAT DAME TO | |
| | CODDECTED NEW HEAT DATE TO | BTU/NKW |
| | | BTU/NKW |
| - T.T.T. | TOTAL HEAT INPUT IS | MMBTU |

1995 Heat Rate Test Results White Bluff Unit Two Page 7

| MEASURED TEST INPUTS FROM FILE 2395b | |
|--|-------------------------------------|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| TEMPERATURE IS | |
| CONDENSER COOLING WATER TEMPERATURE IS | IN-HG LB/HR |
| BACKPRESSURE IS7.03 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM | ક |
| CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS4.98 BPCHG = 2.20 KWCHG = -2.16 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.021570 | 8 |
| THE CORRECTED GROSS GENERATION IS 407.22 | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

1995 Heat Rate Test Results White Bluff Unit Two Page 8

| MEASURED TEST INPUTS FROM FILE 2470a |
|--|
| THE AVERAGE GROSS GENERATION IS |
| CONDENSER IS |
| CONDENSER IS |
| CALCULATED RESULTS |
| THE COOLING TOWER CIRCULATING WATER FLOW IS |
| TEMPERATURE IS |
| CONDENSER COOLING WATER TEMPERATURE IS |
| BACKPRESSURE IS5.42 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION |
| PRESSURE IS |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.017815 % |
| THE CORRECTED GROSS GENERATION IS 494.20 MWe |
| THE CORRECTED NET GENERATION IS 467.80 MWe |
| THE UNCORRECTED NET HEAT RATE IS 10876.5 BTU/NKW |
| THE CORRECTED NET HEAT RATE IS |
| THE TOTAL HEAT INPUT IS |

1995 Heat Rate Test Results

White Bluff Unit Two

Page 9

| MEASURED TEST INPUTS FROM FILE 2470b | |
|--|-------------------------------------|
| THE AVERAGE GROSS GENERATION IS | MWe IN-HG |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F |
| TEMPERATURE IS | |
| CONDENSER COOLING WATER TEMPERATURE IS | LB/HR |
| BACKPRESSURE IS5.28 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | 8 |
| PRESSURE IS3.41 BPCHG = 1.97 KWCHG = -1.93 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.019340 | 8 |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS 11029.9 | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

| 100511 10 1 5 | | | |
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| 1005 Hoot Boto Took Beauty | | | |
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| 1995 Heat Rate Test Results | | | |
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| | ite Bluff Unit Two | | Page 10 |
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| MEASURED TEST INPUTS FROM FILE 2550a | |
|---|---------------------------------|
| THE AVERAGE GROSS GENERATION IS |) MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR |
| | BBL/HR BTU/BBL |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F DEG F IN-HG LB/HR % |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

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| 1995 Heat Rate Test Results | | |
| | White Bluff Unit Two | |
| | | Page 11 |
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| MEASURED TEST INPUTS FROM FILE 2550b | |
|--|-------------------------------------|
| THE AVERAGE GROSS GENERATION IS | MWe |
| CONDENSER IS | DEG F |
| CONDENSER IS | DEG F DEG F PCT LB/HR BTU/LB BBL/HR |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS | DEG F DEG F |
| TEMPERATURE IS | |
| CONDENSER COOLING WATER TEMPERATURE IS | LB/HR |
| BACKPRESSURE IS2.34 THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION | 8 |
| PRESSURE IS2.34 BPCHG = 0.00 KWCHG = 0.00 | 8 |
| THE BACKPRESSURE CORRECTION FACTOR IS | 8 |
| THE CORRECTED GROSS GENERATION IS | MWe |
| THE CORRECTED NET GENERATION IS | MWe |
| THE UNCORRECTED NET HEAT RATE IS | BTU/NKW |
| THE CORRECTED NET HEAT RATE IS | BTU/NKW |
| THE TOTAL HEAT INPUT IS | MMBTU |

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| 1995 Heat Rate Test Results | White Bluff Unit Two | |
| | White Bluff Unit Two | Page 12 |
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| MEASURED TEST INPUTS FROM FILE 2630a | |
|--|---|
| THE AVERAGE GROSS GENERATION IS | |
| CONDENSER IS 118.88 DEG F THE AVERAGE CIRCULATING WATER TEMPERATURE TO THE | |
| CONDENSER IS | R |
| CALCULATED RESULTS | |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. 341000 GPM THE COOLING TOWER RANGE IS. 22.94 DEG F THE DESIGN COLD WATER TEMPERATURE IS. 93.85 DEG F THE DESIGN MAXIMUM COLD WATER TEMPERATURE IS. 95.76 DEG F THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS. 97.85 DEG F THE SATURATION PRESSURE FOR THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS. 3.99 IN-HG THE TURBINE THROTTLE FLOW IS. 4339823.00 LB/HR THE HEAT RATE CORRECTION FACTOR FOR CONDENSER BACKPRESSURE IS1.63 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS1.20 % | |
| BPCHG = 0.44 KWCHG = -0.44 THE BACKPRESSURE CORRECTION FACTOR IS | |
| THE CORRECTED GROSS GENERATION IS | |
| THE CORRECTED NET GENERATION IS 626.23 MWe | |
| THE UNCORRECTED NET HEAT RATE IS 10734.5 BTU/NK | W |
| THE CORRECTED NET HEAT RATE IS 10783.8 BTU/NK | W |
| THE TOTAL HEAT INPUT IS | |

1995 Heat Rate Test Results White Bluff Unit Two Page 13

| MEASURED TEST INPUTS FROM FILE 2630b |
|---|
| THE AVERAGE GROSS GENERATION IS |
| CONDENSER IS |
| CONDENSER IS |
| CALCULATED RESULTS |
| THE COOLING TOWER CIRCULATING WATER FLOW IS. THE COOLING TOWER RANGE IS. 23.07 DEG F THE DESIGN COLD WATER TEMPERATURE IS. 93.87 DEG F THE DESIGN MAXIMUM CONDENSER COOLING WATER THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS. 98.64 DEG F THE SATURATION PRESSURE FOR THE AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE IS. 4.11 IN-HG THE TURBINE THROTTLE FLOW IS. 4393357.00 LB/HR THE HEAT RATE CORRECTION FACTOR FOR CONDENSER BACKPRESSURE IS. -1.37 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION PRESSURE IS. -0.90 % BPCHG = 0.48 KWCHG = -0.47 THE BACKPRESSURE CORRECTION FACTOR IS |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.004742 % |
| THE CORRECTED GROSS GENERATION IS 661.86 MWe |
| THE CORRECTED NET GENERATION IS |
| THE UNCORRECTED NET HEAT RATE IS |
| THE CORRECTED NET HEAT RATE IS 10728.0 BTU/NKW |
| THE TOTAL HEAT INPUT IS |

| 1995 Heat Rate Test Results | | |
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| 1995 Heat Rate Test Results | | |
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| MEASURED TEST INPUTS FROM FILE 2fulla |
|--|
| THE AVERAGE GROSS GENERATION IS |
| CONDENSER IS |
| CONDENSER IS |
| CALCULATED RESULTS |
| THE COOLING TOWER CIRCULATING WATER FLOW IS |
| THE TURBINE THROTTLE FLOW IS |
| THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION |
| PRESSURE IS0.31 % BPCHG = 0.70 KWCHG = -0.70 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.006981 % |
| THE CORRECTED GROSS GENERATION IS |
| THE CORRECTED NET GENERATION IS |
| THE UNCORRECTED NET HEAT RATE IS |
| THE CORRECTED NET HEAT RATE IS |
| THE TOTAL HEAT INPUT IS |

1995 Heat Rate Test Results

White Bluff Unit Two

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| MEASURED TEST INPUTS FROM FILE 2fullb |
|--|
| THE AVERAGE GROSS GENERATION IS |
| CONDENSER IS |
| CONDENSER IS |
| |
| CALCULATED RESULTS |
| THE COOLING TOWER CIRCULATING WATER FLOW IS |
| TEMPERATURE IS |
| THE TURBINE THROTTLE FLOW IS |
| BACKPRESSURE IS1.05 % THE HEAT RATE CORRECTION FACTOR FOR AVERAGE MAXIMUM CONDENSER COOLING WATER TEMPERATURE SATURATION |
| PRESSURE IS0.48 % BPCHG = 0.57 KWCHG = -0.57 |
| THE BACKPRESSURE CORRECTION FACTOR IS 1.005696 % |
| THE CORRECTED GROSS GENERATION IS 727.85 MWe |
| THE CORRECTED NET GENERATION IS |
| THE UNCORRECTED NET HEAT RATE IS |
| THE CORRECTED NET HEAT RATE IS |
| THE TOTAL HEAT INPUT IS |

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| 1995 Heat Rate Test Results | | |
| 1995 Heat Rate Test Results | White Bluff Unit Two | |
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| | | Page 16 |
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COAL HEAT RATE TEST DATA

Plant: White 15/4+

Unit:

| | 96/2/8 96/2/8 | 85/8/ 45/8/ | 841 835 | 396 39.8 | 4,46 4,42 | 125,63 124,64 | 98,84 98,57 | 79.03 76.97 | 160,39 92,76 | 0 | 3658 8398 | 6 6 | | |
|------------------------------|---------------|-------------|----------|----------|-----------------|------------------|-----------------|-------------|----------------|---------------|-----------------|--------------|-----------------|----------------------|
| , , | 8/2/96 | 30841 | 582 | 37.2 | 3,97 | 120.98 | 85,06 | 74,23 | 81,64 | 90808 | 86,15 | 0 | | |
| tions | 8/2/96 | 17504 | 784 | 37.7 | 3,92 | 120.46 | 11.0% | 73,23 | 5966 | 9048CC | 0658 | Э | | |
| Data Needed For Calculations | 96/1/8 | 16508 | 1,89 | 34,2 | 3,45 | 116,32 | 94.74 | 72,30 | 64.76 | 792900 | 8580 | Ð | | |
| Data Ne | 96/1/8 | HOSD/ | 684 | 34,2 | 3.39 | 115,64 | 94.07 | 70.06 | 70,96 | 792500 | 8569 | Ð | | Olspoleine Closse |
| | 96/08/1 | 80551 | 115765 | 28.5 | 4. (4(100) | 124.74 | 92,76 | 73,20 | 14.19 | US4300 | 8475 | ь | | 577 DE |
| | 96/08/2 | 1550A | 815785 | 7.86 | (M)6117 | 1,25,05 | 86'86 | 78.87 | 75.37 | 006589 | 8370 | ¢ | | 848 |
| | Date | File Name | Gross MW | Aux MW | Cond Back Press | Circ Water Out T | Circ Water In T | Wet Bulb T | Dry Bulb T | Coal Flow pph | Coal HHV Btu/lb | Oil Flow bph | Oil HHV Btu/bbl | |

Claim Withdrawn. Contains No CBI. 06/29/2016_YD

Corr Net Ht Rate

Heat In MMBtu Fest Net MW

Corr Gross MW
Corr Net MW
Test Net Ht Rate

COAL HEAT RATE TEST DATA

Plant: White My

| | | | | | | W 2 no agreement | | | | | | | | |
|------------------------------|---------|------------|----------|--------|-----------------|------------------|-----------------|------------|------------|---------------|-----------------|--------------|-----------------|--|
| Data Needed For Calculations | 8/13/96 | 47 9967035 | しんと | 31.6 | 2,96 | 1141 | 92.28 | 60,12 | 72,07 | 662300 | 86.33 | | | |
| Data Neec | 8/13/96 | 1500966 | <u> </u> | 37.8 | 888 | 1/0.18 | 91,45 | 67.32 | 68.61 | | - | | | |
| , | 96/5//2 | ` | ł | 25,4 | 2,00 | 00.801 | 92.17 | 0870 | 65.69 | | 1808 | | | |
| | 96/8/18 | 14500966. | 477 | 256 | 2,64 | 8:201 | 6616 | 69.53 | 82:22 | 543300 | 2637 | | | |
| | Date | File Name | Gross MW | Aux MW | Cond Back Press | Circ Water Out T | Circ Water In T | Wet Bulb T | Dry Bulb T | Coal Flow pph | Coal HHV Btu/lb | Oil Flow bph | Oil HHV Btu/bbl | |

| Outputs | 7672 | 5410.34 | 10330.6 | 10404.2 | 5717.0 | 553.4 |
|---------|---------------|-------------|------------------|------------------|---------------|-------------|
| | 470,22 575,56 | 544.06 | 6'82201 | 10387.6 | 5.451.5 | 552,5 553.4 |
| | 470,22 | 444.82 | 10512,7 | $\overline{}$ | | |
| | 470,73 | 445,13 | 10461,6 | 0.6000 | 4.2617 | 451.4 |
| | Corr Gross MW | Corr Net MW | Test Net Ht Rate | Corr Net Ht Rate | Heat In MMBtu | Test Net MW |

COAL HEAT RATE TEST DATA

Plant: White 5/4+4

| | | | Data Ne | Data Needed For Calculations | ations | | | , |
|------------------|------------|---------|----------|------------------------------|-----------|-----------|-----------|-----------|
| Date | 96/12/2 | | 96/nE/L | 7/30/96 | 96/1/8 | 96/1/8 | 1/3/196 | 1/3/1/46 |
| File Name | 1100A | 1160 12 | 1250 A | 1250E | 1350A | 1350 B | 14504 | 1450K |
| Gross MW | 88/ | | 278 | 100 100 | 373 | 378 | 479 | 472 |
| Aux MW | 24 | | 24,4 | 24,5 | 25,3 | 25.8 | 26,7 | 26,8 |
| Cond Back Press | 2.14 (1pp) | | 2,36(pp) | 2.38(100) | 2,84(100) | 2.78 [00] | 3.29(100) | 2.25(100) |
| Circ Water Out T | 102,94 | | 105.97 | 106,19 | 1/2,4/ | 111,71 | 1116.88 | 1/6.88 |
| Circ Water In T | 88.58 | | 50.88 | 58.13 | 89.89 | 89,29 | 200X | 84.78 |
| Wet Bulb T | 72,44 | | 2//02 | 70.76 | 21.12 | 70.46 | 7///08 | 27.33 |
| Dry Bulb T | 72,90 | | 72,79 | 72,32 | 72,29 | 71.39 | 72,09 | 7247 |
| Coal Flow pph | 265700 | | 355700 | 358700 | 45250 | 4496CD | 208000 | (2)/U/V |
| Coal HHV Btu/lb | 8536 | | 8364 | 8384 | 8683 | 100X | 1000 | 0000 |
| Oil Flow bph | B | | 0 | 9 | 9 | 9 | 000 | 1000 |
| Oil HHV Btu/bbl | | | | | | | 1 | |
| | | | | | | | | |

| | | | Outputs | | | | |
|------------------|----------|----------|---------|----------|---------------|-------------|-----------------|
| Corr Gross MW | 184.36 | 277,85 | 27575 | 3/0/0.02 | P1 162 | 402.60 | 472.60 16.62.62 |
| Corr Net MW | 160,36 | 848.45 | 251.88 | 241.60 | 211.10 215 2d | 11000 | 12787 |
| Test Net Ht Rate | 1,8329.4 | 1/173/14 | 7,724,5 | 1.00211 | 8 19001 | 1811/1 | |
| Corr Net Ht Rate | 14/43.0 | 11934.6 | 11965.7 | 1 1001 | 2 /2/1/ | 0 0000 0000 | A10011 |
| Heat In MMBtu | 2268.0 | 2975.1 | 20078 | 10000 | 28/20 V | 10001 | 100/10/ |
| Test Net MW | 164 | 253.6 | 256,5 | 347,7 | 352,2 | 152,5 | 45.2 |
| | | W 75 75 |) | | | 1 | 801 |

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EQ#
       COEF A
                   COEF B
                                COEF C
                                             R^2
                                                    R^2 C
                                                            EQUATION
     0.5836D+03 0.9645D+01
  1
                              0.0000D+00
                                           0.9976
                                                   0.9974 Y = A + B * X
  2
     0.0000D+00 0.1064D+02 0.0000D+00
                                           0.0000
                                                   0.0000 Y=B*X
  3
     0.4534D-03 -.4616D-06
                             0.0000D+00
                                           0.9005
                                                   0.8934 Y=1/(A+B*X)
     -.1337D+03 0.1045D+02
                             0.1206D+06
                                           0.9992 0.9990 Y=A+B*X+C/X
  5
    0.8416D+04
                -.1158D+07
                             0.0000D+00
                                           0.7834 0.7680 Y=A+B/X
     0.5205D-04
                 0.6534D-01
                             0.0000D+00
                                           0.9825 0.9812 Y=X/(A*X+B)
  7
     0.1227D+05
                -.4016D+07
                             0.3904D+09
                                           0.9654 0.9601 Y=A+B/X+C/X*X
  8
     0.1040D+04
                 0.7287D+01
                             0.2435D-02
                                           0.9995
                                                   0.9995 Y=A+B*X+C*X*X
     0.1193D+02 -.1995D-02
  9
                             0.000D+00
                                           0.0000 0.0000 Y=A*X+B*X*X
 10
     0.3227D+02 0.8259D+00
                             0.0000D+00
                                           0.9925 0.9920 Y=A*X^B
     0.1827D+04 0.1002D+01
 11
                             0.0000D+00
                                           0.9811 0.9798 Y=A*B^X
     0.9757D+04 0.0000D+00
0.2053D+04 0.2792D-03
 12
                             0.0000D+00
                                           0.9056 0.8989 Y=B^{(1/X)}
 13
                             0.0000D+00
                                           0.9727 0.9708 Y=A*X^(B*X)
     0.1158D+05 -.5616D+02
0.1827D+04 0.1997D-02
 14
                             0.0000D+00
                                           0.9305 0.9255 Y=A*X^(B/X)
 15
                             0.0000D+00
                                           0.9811 0.9798 Y=A*e^{(B*X)}
     0.9757D+04 -.2600D+03
 16
                                           0.9056 0.8989 Y=A*e^(B/X)
                             0.0000D+00
 17
     -.1798D+05 0.3835D+04 0.0000D+00
                                           0.9327 0.9279 Y=A+B*lnX
 18
     0.1435D-02 -.1990D-03 0.0000D+00
                                          0.9893 0.9885 Y=1/(A+B*lnX)
 19
     0.1450D+03 0.1001D+01 0.5161D+00
                                           0.9995 0.9994 Y=A*B^X*X^C
 21
     0.9925D+04 0.1139D+04
                                           0.9987 0.9985 Y=A*e^{((X-B)/2)}
                             -.6559D+06
 22
     0.1299D+04 0.3148D+01 0.6692D+01
                                           0.9995 0.9995 Y=A*e^((lnX-B)^2/C)
 24
     0.5858D+04 0.1296D+04
                             0.5161D+00
                                           0.9995 0.9994 Y=A*(X/B)^c*e^(x/b)
 25
     0.8344D-09 -.7610D+03
                             0.1268D-03
                                           0.9910
                                                   0.9896 Y=1/(A*(X+B)^2+C)
BASED ON THE VALUE OF RC( )--BEST FITTING CURVE WAS NUMBER 8
```

With refest of 450 \$ 550 @ 2 circ. pgs.

```
EQ#
       COEF A
                    COEF B
                                 COEF C
                                               R^2
                                                       R^2 C
                                                               EQUATION
     0.6100D+03
                  0.9647D+01
                               0.0000D+00
                                             0.9989
                                                      0.9988 Y = A + B * X
     0.0000D+00
                  0.1069D+02
                                             0.0000
                               0.0000D+00
                                                      0.0000 Y=B*X
     0.4520D-03
                  -.4610D-06
                               0.0000D+00
                                             0.8943
                                                      0.8868 Y=1/(A+B*X)
     0.1043D+03
                  0.1021D+02
                               0.8513D+05
                                             0.9996
                                                      0.9996 Y = A + B * X + C / X
     0.8459D+04
                               0.0000D+00
                  -.1165D+07
                                             0.7924
                                                      0.7776 Y = A + B/X
     0.5047D-04
                  0.6556D-01
                               0.0000D+00
                                             0.9838
                                                      0.9827 Y=X/(A*X+B)
     0.1227D+05
  7
                  -.3992D+07
                               0.3862D+09
                                             0.9712
                                                      0.9668 Y=A+B/X+C/X*X
     0.9104D+03
                  0.8098D+01
                               0.1599D-02
                                                      0.9997 Y=A+B*X+C*X*X
                                             0.9997
     0.1216D+02
                  -.2276D-02
                               0.0000D+00
                                             0.0000
                                                      0.0000 Y=A*X+B*X*X
 10
     0.3201D+02
                  0.8281D+00
                               0.0000D+00
                                             0.9943
                                                      0.9939 Y=A*X^B
 11
     0.1838D+04
                  0.1002D+01
                               0.0000D+00
                                             0.9775
                                                      0.9759 Y=A*B^X
 12
     0.9837D+04
                  0.0000D+00
                               0.0000D+00
                                             0.9108
                                                      0.9044 \text{ Y=B}^{(1/X)}
 13
     0.2066D+04
                  0.2789D-03
                               0.0000D+00
                                             0.9684
                                                      0.9662 Y=A*X^(B*X)
 14
     0.1168D+05
                  -.5641D+02
                               0.0000D+00
                                             0.9352
                                                     0.9306 Y=A*X^(B/X)
 15
     0.1838D+04
                  0.1996D-02
                               0.0000D+00
                                             0.9775
                                                     0.9759 Y=A*e^(B*X)
 16
     0.9837D+04
                 -.2612D+03
                                             0.9108
                               0.0000D+00
                                                     0.9044 \text{ Y=A*e}^{(B/X)}
 17
     -.1803D+05
                  0.3849D+04
                               0.0000D+00
                                             0.9393
                                                     0.9350 Y=A+B*lnX
 18
     0.1436D-02
                 -.1993D-03
                               0.0000D+00
                                             0.9873
                                                     0.9864 Y=1/(A+B*lnX)
 19
     0.1158D+03
                  0.1001D+01
                               0.5630D+00
                                             0.9993
                                                     0.9992 Y=A*B^X*X^C
 21
     0.9437D+04
                               -.5924D+06
                 0.1076D+04
                                             0.9990
                                                     0.9989 Y=A*e^{((X-B)/2)}
 22
     0.1103D+04
                               0.7676D+01
                  0.2734D+01
                                             0.9996
                                                     0.9995 Y=A*e^((1nX-B)^2/C)
 24
     0.7149D+04
                  0.1515D+04
                               0.5630D+00
                                                     0.9992 Y=A*(X/B)^C*e^(x/b)
                                             0.9993
 25
     0.8674D-09
                  -.7503D+03
                               0.1266D-03
                                             0.9916
                                                     0.9904 Y=1/(A*(X+B)^2+C)
BASED ON THE VALUE OF RC( )--BEST FITTING CURVE WAS NUMBER 8
```

WB #1 before no testing 450 = 550 loads

| 9608011000, | 165300. | 162700 | Λ | 157300 | 165000 | 45100 | 165000 | 0 111110111 | momr | 100 | •* |
|--|---------|---------|---|---------|---------|---|--|---------------------------------------|--------|--------------|-----|
| 9608011100, | 163700 | 161000 | ο, | 15/300, | 162500 | 150000 | 163900, | O,UIHKLY | TOTL= | 430.65 TONS | |
| 9608011200, | 161800 | 159200 | ο, | 155600 | 161600 | 157100 | 164300 | , U,UIHRL | TOTL= | | |
| <u>69608011300</u> , | 164000. | 161400 | n, | 153600, | 162000, | 150400 | 162500 | , U,UIHRL | TOTL= | 478.9 TONS | |
| 19608011400, | 164100 | 162200 | 0 | 151400 | 164600 | 109400, | 164700 | O.UIHRL | TOTL= | | |
| 29608011500, | 163400. | 160700 | n, | 157600 | 162100 | 150000 | 160000 | O,UIHRLY | TOTL= | 483.95 TONS | |
| 39608011600. | 162700 | 160100, | ο, | 157600, | 163100, | 150100 | 164000 | , O,UIHRL | TOTL= | | |
| 49608011700, | 157400 | 154800 | | 165200 | 157400 | 150000 | 153400 | U, UIHRLY | TOTL= | 482.2 TONS | |
| 9608011800 | 156700 | 154000, | 0, | 166600 | 15/400, | 152900, | 158100 | , U,U1HRLY | TOTL= | 472.95 TONS | |
| ⁵ 9608011800, 9 608011900, | 156900 | 154100, | 0, | 167500 | 156500, | 152100, | 157400, | 0,U1HRLY | TOTL= | 471.7 TONS | |
| ⁷ 9608012000, | 157500 | 154900 | 0. | 166000 | 157400 | 152300, | 15/500 | O.UIHRLY | TOTL= | 472.65 TONS | |
| *9608012100 | 157700 | 155100 | ο, | 160900, | 157400, | 152900, | 158300, | O,UIHRLY | TOTL= | 473.95 TONS | |
| 9608012100, | 160400 | 157000 | ٥, | 161600 | 107600, | 153100, | 158300 | O,UIHRLY | TOTL= | 475.5 TONS | ¥ |
| *9608012200. | 162900 | 160100 | 0. | 164500 | 160100. | 155700, | 161100 | O.U1HRLY | TOTL= | 478.05 TONS | |
| *9608012300, | 160100 | 157500 | 0, | 164500, | 152500, | 158100, | 163500 | O,UIHRLY | TOTL= | 485.85 TONS | |
| 119608020000, | 149000 | 146300 | υ, | 100000, | 159800, | 155400, | 160700, | 0,U1HRLY | TOTL= | 480.05 TONS | |
| 129608020100, | 140400 | 120000 | <u>, , , , , , , , , , , , , , , , , , , </u> | 167000, | 148800, | 144400. | 149700 | 0.U1HRL | TOTL= | 452.55 TONS | |
| 13 9608020200, | 121200 | 130000, | υ, | 167100, | 140400, | 136100, | 141300, | 0,U1HRLY | TOTL= | 431.65 TONS | |
| 149608020300, | 117600 | 115500 | υ, | 161300, | 131400, | 127000, | 132200, | 0,U1HRLY | TOTL= | 406.05 TONS | |
| 15 9608020400. | 111600. | 110000. | Ň. | 125000. | 117900. | 113700, | 101800, | 0.U1HRLY | TOTL= | 345.75 TONS | |
| 169608020500, | 111000, | 109500, | υ, | 108500, | 112100, | 107800, | 112900, | 0,U1HRLY | TOTL= | 331.2 TONS | |
| 179608020600, | 140500, | 123900, | Ο, | 128900, | 126400, | 122100, | 127200, | 0,U1HRLY | TOTL= | 377.35 TONS | |
| 189608020700, | 151000 | 147000. | 0. | 146100, | 149300, | 144900, | 150200. | 0.U1HRLY | TOTL= | 443.5 TONS | |
| J000020000, | 101000, | 140400, | υ. | 154000. | 150900. | 146400 | 151700 | A HILLDEN | ጥለጥ፤ - | 451.2 TONS | |
| 3000020300, | 101000, | 148900, | υ, | 152800. | 151300. | 146900. | 1522m | O HIMPIN | ጥርም፣ - | 451.8 TONS | |
| 3000041000. | 149200. | 146700. | · (). | 151900. | 149100 | 144600 | 150000 | O DISTRIBUTA | mom t | 445.75 TONS | , |
| ² 9608021100, | 152300, | 149700, | 0, | 150100, | 152100, | 147700, | 152900, | 0,U1HRLY | TOTL= | 452.4 TONS 9 | 048 |
| ²³ 9608021200, | 152900, | 150300, | Ο, | 151000, | 152800, | 148400, | 153600, | 0,U1HRLY | TOTL= | 454.5 TONS | |
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| 28 29 30 31 31 32 33 34 35 36 37 36 39 40 41 42 43 44 45 46 47 48 49 50 51 | | | | | | | | | | | |
| 28 29 30 31 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 56 51 52 53 | | | | | | | | | | | |

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9607310000, 0, 32800, 105300, 100, 80600, 78500, 700, 0, U1HRLY TOTL= 149 TONS 9607310100, 0, 30000, 80300, 0, 74700, 0, 0, 0, U1HRLY TOTL= 92.5 TONS 9607310200, 0, 91300, 85100, 0, 82300, 0, 0, 0, U1HRLY TOTL= 129.35 TONS 9607310300, 0, 94800, 88500, 0, 82400, 0, 0, 0, U1HRLY TOTL= 132.85 TONS 2657 9607310400, 0, 38800, 36200, 0, 64000, 0, 0, 0, U1HRLY TOTL= 69.5 TONS 9607310500, 0, 63000, 60600, 0, 133800, 0, 0, 0, U1HRLY TOTL= 128.7 TONS 9607310600, 0, 147300, 145900, 0, 149600, 0, 103300, 0, U1HRLY TOTL= 273.05 TONS 9607310700, 0, 143200, 136600, 0, 145600, 0, 145300, 0, U1HRLY TOTL= 285.35 TONS 9607310800, 0, 142300, 135700, 0, 144500, 0, 144300, 0, U1HRLY TOTL= 283.4 TONS 5665.
```

| 1 500 |), 164700, 16 9608021400 | 80200, 16 | 55600, 0, | U1H | RLY TOTI | = 483.2 | 5 TONS | | | | |
|--------------|------------------------------|--|--|--------------|----------------|---------|--|--|---------------------------------------|--|--------------------------|
| | | | | | | | | 169300. | O.HIHRLY | ተርሞ፣ – | 491.9 TONS |
| | 9608021500, e9608021600, | 166100, | 163500, | 0, | 150300, | 165900, | 161300, | 166700, | 0.U1HRLY | TOTL= | 491.9 TONS 486.9 TONS |
| | 69608021600, 19608021700, | 165300 | 163500, | <u>, 0, </u> | <u>149900,</u> | 166000, | 161500, | 166800, | 0,U1HRLY | TOTL= | 487 TONS 9740. |
| ` + | | 100000, | 102700, | υ, | 152000, | 165000, | 160500, | 161600, | 0,U1HRLY | TOTL= | 483.55 TONS |
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9607311000, 120500, 167200, 160600, 0, 169400, 72400, 169300, 0, U1HRLY TOTL= 429.7 TONS
9607311100, 165200, 162700, 156100, 0, 165100, 160600, 164700, 0, U1HRLY TOTL= 487.2 TONS
9607311200, 164400, 161900, 155300, 0, 164300, 159700, 164000, 0, U1HRLY TOTL=
                                                                               484.8 TONS
9607311300, 167400, 164800, 158200, 0, 167200, 162600, 157700, 0, U1HRLY TOTL=
                                                                              488.95 TONS
9607311400, 174300, 171700, 165100, 0, 174000, 169500, 124600, 0, U1HRLY TOTL=
                                                                               489.6 TONS
9607311500, 163700, 161200, 154600, 0, 163600, 159100, 164400, 0, U1HRLY TOTL=
                                                                               483.3 TONS
9607311600, 164800, 162300, 155700, 0, 164700, 160100, 165500, 0, U1HRLY TOTL=
                                                                               486.55 TONS
9607311700, 164000, 161400, 154800, 0, 163900, 159300, 164700, 0, U1HRLY TOTL=
                                                                               484.05 TONS
9607311800, 163400, 160900, 154200, 0, 163300, 158800, 164000, 0, U1HRLY TOTL=
                                                                               482.3 TONS
9607311900, 162800, 160300, 153700, 0, 162700, 158100, 163500, 0, U1HRLY TOTL=
                                                                               480.55 TONS
9607312000, 161600, 159000, 152400, 0, 161500, 156900, 162200, 0, U1HRLY TOTL=
                                                                               476.8 TONS
9607312100, 160600, 158100, 151600, 0, 160500, 156100, 161400, 0, U1HRLY TOTL=
                                                                              474.15 TONS
9607312200, 159700, 157100, 150500, 0, 159600, 155000, 160400, 0, U1HRLY TOTL= 471.15 TONS
9607312300, 135800, 133600, 127000, 0, 136000, 131600, 136800, 0, U1HRLY TOTL= 400.4 TONS
9608010000, 115500, 13600, 105300, 0, 114500, 45900, 115200, 0, U1HRLY TOTL= 255 TONS
9608010100, 115400, 0, 106800, 0, 115800, 0, 116700, 0, U1HRLY TOTL= 227.35 TONS
9608010200, 115100, 0, 106400, 0, 115500, 0, 116300, 0, U1HRLY TOTL=
                                                                     226.65 TONS
9608010300, 114900, 0, 106300, 0, 115200, 0, 116100, 0, U1HRLY TOTL= 226.25 TONS 4525P
9608010400, 114100, 0, 105500, 0, 114600, 0, 115400, 0, U1HRLY TOTL= 224.8 TONS 4496.
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| È | 9608010500, | 139000 | 26600 | 6316 | nn. 8880 | 0. 13900 | 0. 0 | 13990 | o, o,uihri | LY TOTL: | = 298.2 | 2 T | |
| | 9608010300, | 150000, | 157100 | 001 | 159500 | 159500 | ń. | 160400. | O.UIHRLY | TOTL= | 397.65 | TO | |
| \$ | 9608010600, | 139800, | 157100, | ο, | 150500, | 1503000, | Λ, | 160200 | O HIHRLY | TOTL= | 397.5 | ON | |
| <u></u> | 9608010000, | 159700, | 157000, | 0, | 158600, | 159400, | υ, | 150000, | O HIMDIV | TOTE- | 396.25 | TO 79 | 125 |
| | 69608010800, | 158100, | <u> 155600,</u> | <u>0,</u> | 161900, | 158000, | <u>U, </u> | 158900, | U,UIHKLY | TOIL- | 350.25 | | 220 |
| 差. | 9608010900, | 159200, | 156500, | 0, | 158600, | 158800, | О, | 159800, | 0,U1HRLY | TOTL= | 396.45 | TO | 121 |
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| 1 | 33 | | | | | | | | | | | | |
| • | | | | | | | | | | | | | |
| E | 34 | | | | | | | | | | | • | |
| | | | | | | | | | | | | | |

(



Inter-Office Correspondence

TO:

Jim Campbell

T-EP-16

Mike Bakewell

T-EP-16

Lynn Sanders William Phillips

A-WB A-SOC

Henry Thompson

A-TCBY-23G

Al Ralston

A-SOC

FROM:

Roger Lawson

Phone 8-764-7329

Pat Klepper

Phone 8-762-4529

DATE:

8/20/96

SUBJECT:

1996 White Bluff Plant - Heat Rate Test Results

A series of heat rate tests were performed on both White Bluff Units starting July 30 and ending August 13. Co-owners were notified prior to the testing and representatives from Arkansas Electric Cooperative were present to observe the testing. Testing was performed in an unbiased manner.

Each unit was tested from 160 net MW through full load. Unit One's heat rate improved throughout the load range when compared to last year. Unit Two's heat rate improved at all loads below 750 net MW. Both high pressure heater trains on Unit Two were isolated on this and last years' tests. The hot and cold end air heater baskets on Unit Two were replaced last Fall.

The coefficients for the 1996 heat rate curves are;

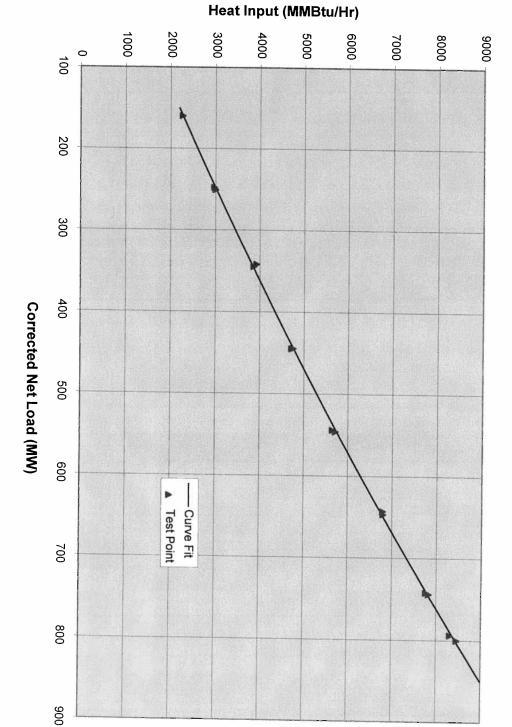
| Term | Unit One | Unit Two |
|------------------|----------|----------|
| \mathbf{X}^2 | 0.002435 | 0.003001 |
| \mathbf{X}^{1} | 7.2870 | 6.9714 |
| X^0 | 1040.431 | 1117.698 |

We recommend that these results be implemented for dispatch and co-owner billing.

The complete results are presented as charts on an the EXCEL spreadsheet "WBHR1996.XLS" which was sent via. cc:mail along with this memo.

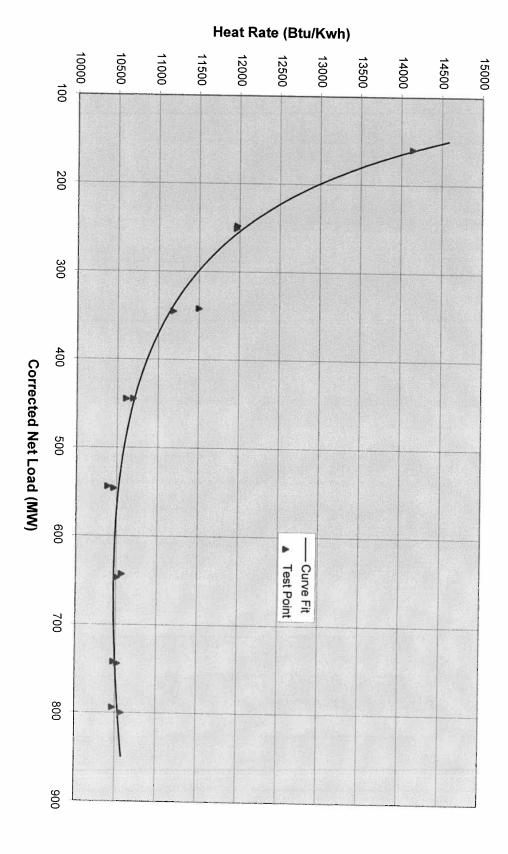
cc: George Eubanks A-WB-SC

David Harris A.E.C.C.

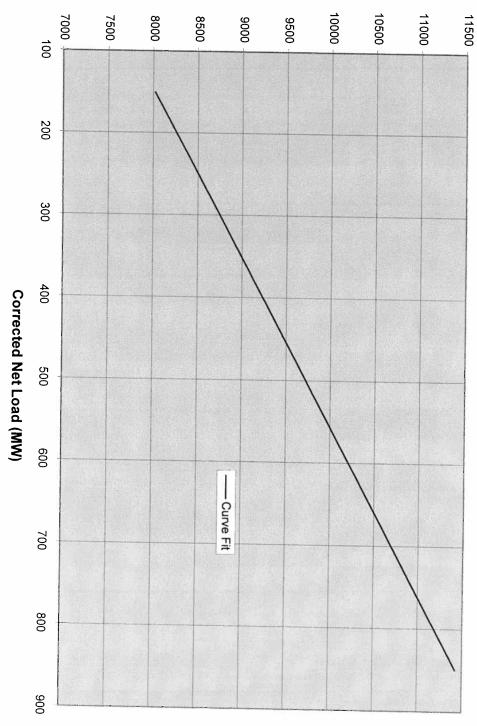


1996 White Bluff Unit 1 Heat Rate

1996 White Bluff Unit 1 Heat Rate

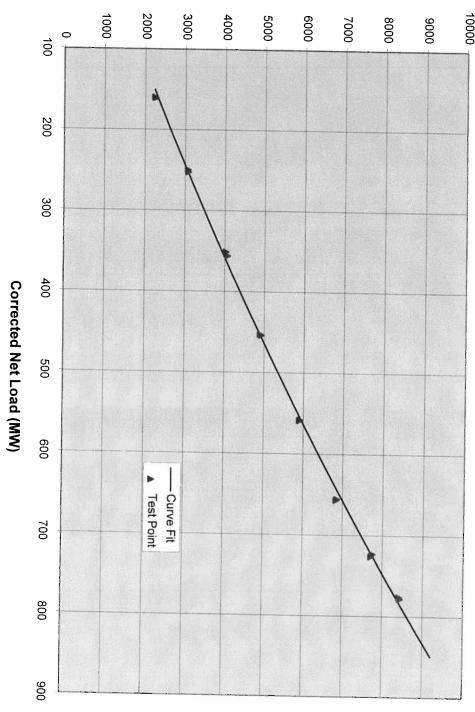


Incremental Heat Rate (Btu/Kwh)



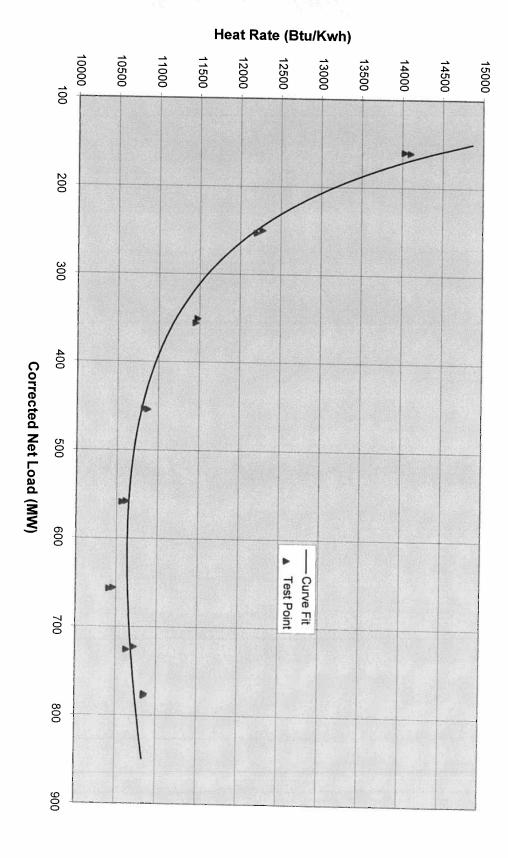
1996 White Bluff Unit 1 Heat Rate

Heat Input (MMBtu/Hr)

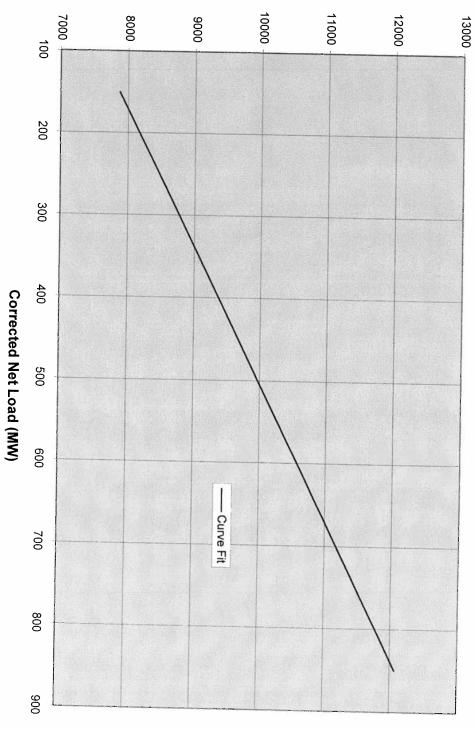


1996 White Bluff Unit 2 Heat Rate

1996 White Bluff Unit 2 Heat Rate



Incremental Heat Rate (Btu/Kwh)



1996 White Bluff Unit 2 Heat Rate

COAL HEAT RATE TEST DATA

Plant: Unite 15/14

| | | | Data Ne | Data Needed For Calculations | ations | , , | | |
|------------------|--------|--------|---------|------------------------------|--------|--------|--------|--------|
| Date | 16/2/8 | 96/5/8 | 96/9/8 | 96/9/8 | 96/4/8 | 8/1/96 | 8/2/96 | 2/2/66 |
| File Name | 2/60A | 21608 | AZSOA | 80522 | 2350A | 2350B | 2450 A | 2450B |
| Gross MW | 186 | 181 | 280 | 218 | 788 | 380 | 481 | 482 |
| Aux MW | 23,5 | 23.9 | 24.6 | 24.7 | 8156 | 25.0 | 26,3 | 261 |
| Cond Back Press | 1811 | 08// | 21.14 | 1118 | 777 | 2,40 | 2,20 | 8,39 |
| Circ Water Out T | 46,06 | 16,71 | 101,54 | 101.12 | 01:501 | 104.42 | 108.42 | 109,45 |
| Circ Water In T | 11.68 | 88,84 | 80.06 | 90.37 | 51.179 | 90.54 | 91.47 | 9248 |
| Wet Bulb T | 14,39 | 74.16 | 73.70 | 73,66 | 73,72 | 72,60 | 74.00 | 75.33 |
| Dry Bulb T | 78,30 | 12.77 | 77.32 | 7706 | 76.24 | 75.95 | 76.15 | 78,72 |
| Coal Flow pph | 256100 | 259400 | 350400 | 356100 | 485100 | 482100 | 576300 | 575100 |
| Coal HHV Btu/lb | 8780 | - | 1508 | 8637 | 8398 | 8362 | 8504 | 8888 |
| Oil Flow bph | | | | | | | | |
| Oil HHV Btu/bbl | | | | | | | | |
| | | | | | | | | |

| | | | | Outputs | | | | |
|------------------|---------|---------|----------|---------|---------|---------|---------|---------|
| Corr Gross MW | 183,75 | 184,73 | 22775 | 27275 | 36'088 | 374,26 | 478.88 | 480,25 |
| | 160.25 | 140,83 | 252,62 | 250.53 | 997558 | 351.26 | 452,58 | 454.15 |
| Test Net Ht Rate | 13837.3 | 1390814 | 12072.1 | (2/42.3 | 825811 | 11355.8 | 107782 | 10829.6 |
| Corr Net Ht Rate | 14031.6 | 14104.4 | 12205.1. | 122766 | 11454.3 | 11476.8 | 10828.6 | 108744 |
| Heat In MMBtu | 2248.6 | 226815 | 30837 | 30756 | 4073.9 | 4031.3 | 4900.9 | 4987.2 |
| | 16215 | 1631 | 255,4 | 2.55 | 358.7 | 355,0 | 454,7 | 455,9 |

COAL HEAT RATE TEST DATA

riant: Unite Di

Unit:

| | , | | Data Ne | Data Needed For Calculations | tions | | | , , |
|------------------|--------------|--------------|---------|------------------------------|--------|----------|--------|--------|
| Date | 26/0/2 | 96/0/8 | 96/4/8 | 96/6/8 | 26/8/8 | 96/8/8 | 26/8/8 | 8/8/4 |
| File Name | 2550H | 25508 | 265A | 26506 | 27264 | 27208 | 2780A | 2780B |
| Gross MW | 588 | SSS | 069 | 889 | 00/2 | 424 | 8/2 | 8/5 |
| Aux MW | 28:3 | 28,2 | 30.3 | 2012 | 33,9 | 33,8 | 36,2 | 36,2 |
| Cond Back Press | 2,454 | 2,540 | 19:8 | 2.40 | 3,42 | 2.42 | 3,42 4 | 3,49 A |
| Circ Water Out T | 112.79 | 113.43 | 78'5// | 115.44 | 122.67 | 122,53 | 124.80 | 123,97 |
| Circ Water In T | 72,60 | 93.20 | &£'16 | 92102 | 46.34 | 96,27 | 94,77 | 95:56 |
| Wet Bulb T | 74,25 | 75,66 | 22,27 | 73.45 | 77.62 | 78,33 | 77,90 | 77.35 |
| Dry Bulb T | 76,49 | 78,86 | 74,22 | 74,33 | 87.12 | 30.45 | 41.54 | 84,70 |
| Coal Flow pph | 702000 | 692700 | 001003 | az 2008 | 89580 | 18962B | 3000 | 975000 |
| Coal HHV Btu/lb | 8434 | XXXX | £87% | 8003 | Stolen | 8743 | 6818 | 701/8 |
| Oil Flow bph | | | | | (8620) | (8/05/1) | | |
| Oil HHV Btu/bbl | | | | | | | | |
| | Large spread | 11 4 x B BP& | | | | | | |
| | ~ | | | | | | | |

| | WW. | | | | | | | |
|------------------|--------|----------|------------|---------|----------|---------|---------|----------|
| | | | | Outputs | | | | |
| Corr Gross MW | 96585 | 06'285 | 487,44 | 18.589 | 760,00 | 757,00 | 8/7/8 | 14,24 |
| Corr Net MW | 99755 | 558,70 | 1057,14 | L | 726.10 | 723,20 | 275.80 | 70800 |
| Test Net Ht Rate | | 10545.2 | 10373.3 | | 10/03/46 | 10727.9 | 9,65801 | 1 |
| Corr Net Ht Rate | 021001 | 10565.91 | \ <u>`</u> | 1 | 106346 | 472701 | | 10884. P |
| Heat In MMBtu | 5920.7 | 5903.2 | | 6860.2 | 7721.8 | 7.88.4 | 8424,9 | 8445,5 |
| Test Net MW | 2867 | 8655 | 1,650 | 81250 | 726.1 | 723,2 | 775.8 | 772.8 |

```
EQ#
       COEF A
                    COEF B
                                 COEF C
                                              R^2
                                                      R^2 C
                                                               EQUATION
 1
     0.5766D+03
                  0.9818D+01
                              0.0000D+00
                                                     0.9959 Y=A+B*X
                                            0.9962
     0.0000D+00
                  0.1081D+02
                               0.0000D+00
                                                     0.0000 Y=B*X
                                            0.0000
  3
     0.4548D-03
                 -.4722D-06
                              0.0000D+00
                                            0.8980
                                                     0.8907 Y=1/(A+B*X)
  4
     -.1257D+03
                                            0.9976
                  0.1062D+02
                               0.1164D+06
                                                     0.9972 Y = A + B * X + C/X
  5
     0.8485D+04
                 -.1161D+07
                                            0.7949
                               0.0000D+00
                                                     0.7802 Y = A + B/X
  6
     0.4865D-04
                  0.6556D-01
                               0.0000D+00
                                            0.9883
                                                     0.9875 Y=X/(A*X+B)
  7
     0.1227D+05
                 -.3967D+07
                                            0.9629
                               0.3822D+09
                                                     0.9572 Y = A + B/X + C/X * X
  8
     0.1118D+04
                  0.6971D+01
                               0.3001D-02
                                            0.9988
                                                     0.9986 Y=A+B*X+C*X*X
  9
     0.1207D+02
                  -.1980D-02
                               0.0000D+00
                                            0.0000
                                                     0.0000 Y = A * X + B * X * X
 10
     0.3185D+02
                  0.8302D+00
                               0.0000D+00
                                            0.9940
                                                     0.9936 Y=A*X^B
 11
     0.1821D+04
                  0.1002D+01
                               0.0000D+00
                                            0.9806
                                                     0.9792 Y=A*B^X
 12
     0.9904D+04
                  0.0000D+00
                               0.0000D+00
                                            0.9166
                                                     0.9107 Y=B^{(1/X)}
 13
     0.2048D+04
                 0.2856D-03
                              0.0000D+00
                                            0.9725
                                                     0.9706 Y=A*X^(B*X)
     0.1175D+05
                 -.5629D+02
                               0.0000D+00
                                            0.9392
                                                     0.9348 Y=A*X^(B/X)
 15
     0.1821D+04
                 0.2037D-02
                              0.0000D+00
                                            0.9806
                                                     0.9792 Y=A*e^(B*X)
 16
     0.9904D+04
                 -.2606D+03
                              0.0000D+00
                                            0.9166
                                                    0.9107 Y=A*e^(B/X)
 17
     -.1801D+05
                  0.3850D+04
                              0.0000D+00
                                            0.9347
                                                     0.9301 Y=A+B*lnX
 18
     0.1441D-02
                 -.2004D-03
                              0.0000D+00
                                            0.9867
                                                     0.9858 Y=1/(A+B*1nX)
 19
     0.1276D+03
                 0.1001D+01
                              0.5433D+00
                                            0.9995
                                                     0.9995 Y=A*B^X*X^C
 20
     0.5319D+01
                 0.2380D+38
                                                     0.9987 Y=A*B^{(1/X)}*X^C
                              0.1087D+01
                                            0.9988
 21
     0.9855D+04
                  0.1114D+04
                                            0.9973
                               -.6276D+06
                                                     0.9968 Y=A*e^{((X-B)/2)}
 22
     0.1130D+04
                  0.2795D+01
                                            0.9992
                              0.7480D+01
                                                     0.9991 Y=A*e^((1nX-B)^2/C)
 24
     0.6484D+04
                  0.1379D+04
                               0.5433D+00
                                            0.9995
                                                     0.9995 Y=A*(X/B)^C*e^(x/b)
 25
     0.8953D-09
                  -.7380D+03
                               0.1286D-03
                                                     0.9857 Y=1/(A*(X+B)^2+C)
                                            0.9876
BASED ON THE VALUE OF RC( ) -- BEST FITTING CURVE WAS NUMBER 19
```

CITE AND 1450B97 487 480.45 28.3 8080 58. 100 م ربا 4906.668 493.8. 10850 4. 4. 2202 (NWW) 6.31 0 SSOB9 8-18-8 380.3 COAL HEAT RATE TEST DATA 55,000 1250A 9 後の、ひめ Q, Walter Data Needed For Calculations 180897 Outputs 1040.5054 7.298 (NING)+ ロシンクな 49-61-8 のらら 250 A9 347700 71017 456, 10897 V (249337 X00X でつこつ 10 No. 3936 3718 79. 127 140497 8888 Ì N.A. a \widetilde{M} File Name . DA7 Coal HHV Btu/lb Corr Net Ht Rate Circ Water Out T Oil HHV Btu/bbl Test Net Ht Rate Cond Back Press Heat In MMBtu Corr Gross MW Coal Flow pph Circ Water In T Corr Net MW Test Net MW Oil Flow bph Wet Bulb T Dry Bulb T Gross MW Aux MW Unit:

COAL HEAT RATE TEST DATA

Tailt:

| | | | Data Ne | Data Needed For Calculations | ations | | | |
|------------------|---------|-------------|----------------------------------|------------------------------|----------|---------|--|-----------|
| Date | 66-81-8 | 1.6.21-8 | 16-13-07 8-13-97 8-14-97 8-14-97 | 18-18-97 | 16-41-8 | 16-11-8 | 1641-8 | 6-14-20 |
| File Name • D/+T | 1955/ | 1550B97 | 16200301 | 1620897 | 1750497 | 1450897 | 1FULLA97 | 1FULL8 97 |
| Gross MW | 588 | い め り | 688 | 889 | 785 | 183 | 870 | 860 |
| Aux MW | 30.6 | 30,8 | 88.8 | 33,1 | 00 in | 37.0 | 40,1 | 40.7 |
| Cond Back Press | 3,24 | 3.37 | 3,96 | 3,96 | 4.76 | 4.56 | 4,75 | 4.88 |
| Circ Water Out T | 112,76 | 113.86 | 491181 | 021161 | 124.92 | 123.50 | 124,16 | 125.88 |
| Circ Water In T | 05.57 | 95.62 | 56.001 | 18.001 | 101.21 | 18.001 | 94,75 | 97,02 |
| Wet Bulb T | 75.17 | 76.29 | 91.92 | 76.69 | 79,73 | 79,63 | 77.16 | 78.47 |
| Dry Bulb T | 77.46 | 78.75 | 18.66 | 81.34 | 93,28 | 1821.76 | 84,88 | 87.07 |
| Coal Flow pph | 648000 | 653300 | 0000066 | 001811 | (00891/8 | 20081X | 98630 | 982SO |
| Coal HHV Btu/lb | 87.20 | 1968 | 0008 | 1658 | 8880 | 980 W | 8772 | 8743 |
| Oil Flow bph | | | | | | | | |
| Oil HHV Btu/bbl | | | | | | | West of the second seco | |
| | | | | | | | | |

| | | | | Outputs | | | | |
|------------------|---------|----------|------------------|--------------|--------------|----------|----------|----------|
| Corr Gross MW | 1885 | 5.83.00 | 08-289 | のたちゅう | 787,25 | 784,17 | 16.808 | 200 |
| Corr Net MW | | 552.26 | 647,30 | 954,10 | 50756 | 747,17 | 10,000 | 878'W |
| Test Net Ht Rate | 618 | 10528 | 10201 | 10201 | 86801 | 2720/ | 52401 | 10371 |
| Corr Net Ht Rate | - 1 | 10364 | 10336 | 10220 | 29801 | 10344 | 10,439 | 10371 |
| Heat In MMBtu | 568.560 | 5925,500 | 10690,716 | 6684,657 | 786 5816 | 7729,034 | 8651.824 | 8289,998 |
| Test Net MW | 554,4 | 574.2 | 649.5 | 654.9 | 748.8 | 745.0 | 829.9 | 828.3 |
| 414 In | - 998. | 7-129 | WINN) E83 (WINN) | + | 2061 F. p. f | 1900 M | 10/30 | (450A) |



Inter-Office Correspondence

TO:

Tom Schnatz Mike Bakewell Lynn Sanders George Eubanks

Al Ralston **Tony James** Henry Thompson **T-EP-17B**

T-EP-17B A-WB

A-WB-SC T-PKWD-3F

T-PKWD-3F T-PKWD-3H

FROM:

Roger Lawson

Phone 8-764-7329 Pat Klepper Phone 8-762-4529

DATE:

8/28/97

SUBJECT:

1997 White Bluff Plant - Heat Rate Test Results

A series of heat rate tests were performed on both White Bluff Units starting July 7 and ending August 14. Co-owners were notified prior to the testing and representatives from Arkansas Electric Cooperative were present to observe the testing. Testing was performed in an unbiased manner.

Each unit was tested from 160 net MW through full load. Unit One's heat rate improved throughout the load range when compared to last year. Unit Two's heat rate improved at all loads above 550 net MW. Last year both high pressure heater trains on Unit Two were isolated during the tests, this year they were not isolated.

This years test were performed with one circulating water pump operation at minimum load on both units. Unit 1 was also tested with one pump operation at 250 MW. The first hour test at 450 MW on Unit 1 was performed with one circ water pump operation and the second hour test with two pump operation. Operating the second pump increased the auxiliary usage by 3.3 MW, but this was more than offset by the 0.6 inch decrease in back pressure at the ambient conditions during the test. The resulting decrease in heat rate with both pumps operating was 400 Btu/Kwh. The difference is shown on the attached charts.

The heat input at each of the corrected test loads is shown in the following table.

| Corrected Test | Load (Net MW) | Heat Input (| MMBTU/Hr) |
|----------------|---------------|--------------|-----------|
| <u>Unit 1</u> | Unit 2 | Unit 1 | Unit 2 |
| 157.30 | 158.58 | 2192.171 | 2261.267 |
| 160.63 | | 2193.247 | , |
| 255.27 | 247.17 | 3076.450 | 3033.339 |
| 256.29 | 251.16 | 3137.645 | 3050.726 |
| 354.83 | 346.49 | 3952.458 | 3970.887 |
| 355.22 | 347.22 | 4032.971 | 4097.542 |
| | 450.00 | | 4925.064 |
| 458.15 | 454.66 | 4819.796 | 4910.500 |
| 551.61 | 547.42 | 5650.560 | 5888.830 |
| 552.26 | 552.36 | 5723.561 | 5861.807 |
| 647.30 | 647.54 | 6690.716 | 6743.269 |
| 654.10 | 649.27 | 6684.657 | 6875.606 |
| 747.17 | 753.20 | 7729.034 | 7849.489 |
| 751.05 | 756.10 | 7785.984 | 7921.463 |
| 828.30 | 853.31 | 8589.998 | 8915.273 |
| 828.81 | 855.13 | 8651.824 | 8941.020 |

The coefficients for the 1997 heat rate curves are:

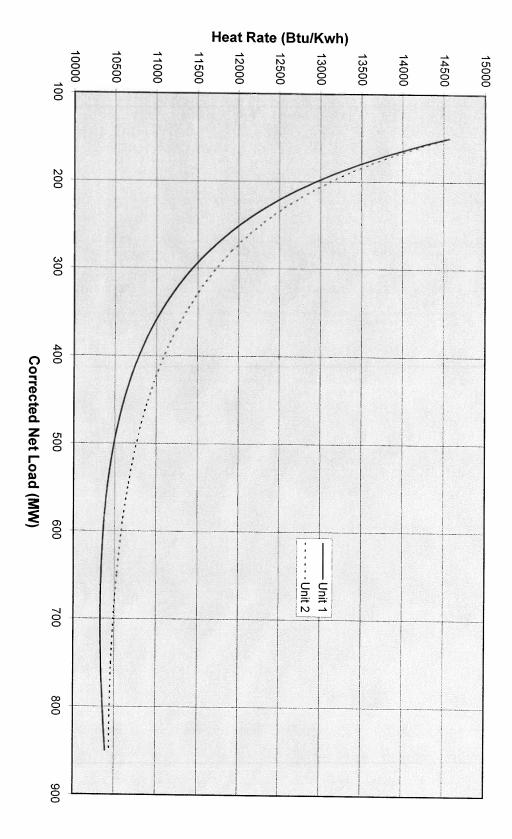
| Term | Unit 1 | Unit 2 |
|-------------------|-------------------------------|-------------------------------|
| X^2 X^1 X^0 | 0.002202 7.298 1040.565 | 0.001217 8.3394 907.130 |

We recommend that these results be implemented for economic dispatch and co-owner billing.

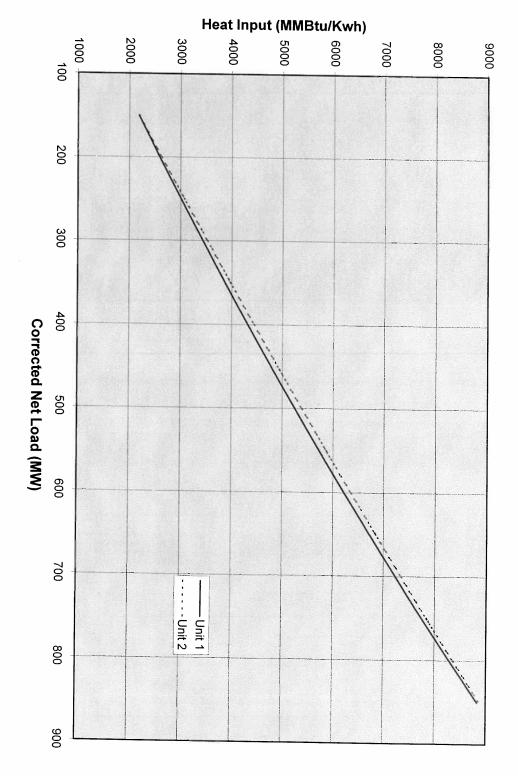
The complete results are presented as charts on an the EXCEL spreadsheet "WBHR1997.XLS" which is a cc:mail attachment along with this memo.

cc: David Harris A.E.C.C.

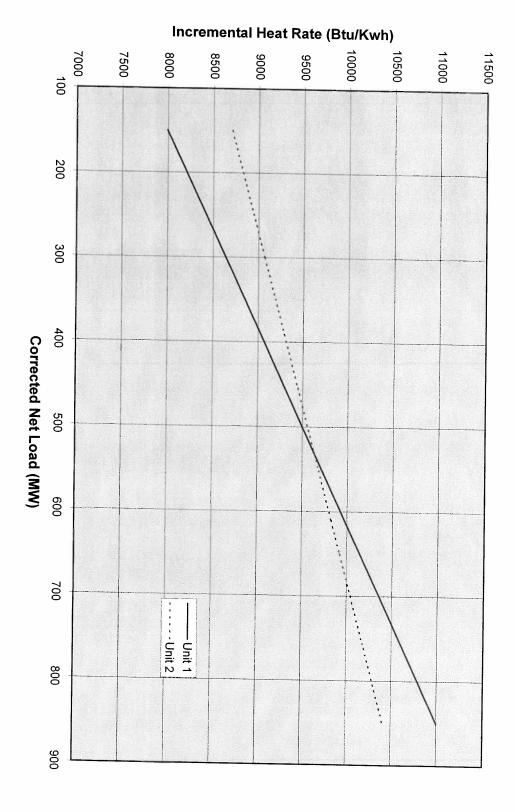
1997 White Bluff Heat Rate



1997 White Bluff Heat Rate



1997 White Bluff Heat Rate



20, 6, 10099 1 81 250 8 (NOW) + 20 1233 (NOW) =

COAL HEAT RATE TEST DATA

Plant: US

| | 300 | | | 1000 | : | 119.28 | | |
|------------------|----------|---|-----------|------------------------------|---------|-----------|-----------------|---|
| | 2000 | 1.34.36 | | | 118,58 | 1:113 | 1 Circ who pume | 2 |
| | | , | Data N | Data Needed For Calculations | tions | | | |
| Date | 1/1/97 | 16/11/6 | 1.6/8/1 | 48/12 | 48/8/1 | 16/8/2 | 719197 | |
| File Name DAT | 2350 AT | 7350897 | 79402497 | 2450BP1 | んかかんかん | 2521697 | 2110407 | |
| Gross MW | 379 | 377 | 481 | 486 | V&V. | クロン | 1 1 1 | |
| Aux MW | 24,5 | 24.3 | 2018 | みがみ | 7.80 | 180 | 7.78 | |
| Cond Back Press | 2,332,24 | 2.24 2.21 | 2,79 2.76 | 0.0 | 3/2 20 | 2 19 3.08 | 87 200 | |
| Circ Water Out T | 102,78 | 25'101 | 1842 | 108.14 | CX!!! | 112.51 | 100,20 | |
| Circ Water In T | 89°68 | 88,39 | 92,25 | 93,03 | 92,69 | 92,46 | 100 TX | |
| Wet Bulb T | 27.89 | 68.68 | 8576 | 77,30 | 62.53 | 28.00 | 12.70 | |
| Ory Bulb T | 72,74 | 71,79 | 45,54 | 73,94 | 74.69 | 0000 | 1800 | |
| Coal Flow pph | 2864 | 4829D | NXXXX | したのでなどののためなり | 1070000 | CON111 | クトログラウ | |
| Coal HHV Btu/lb | 8347 | 8223 | 8366 | 2772 | 8633 | 1000 X | 877.8 | |
| Oil Flow bph | | | | | | 1750 | 0010 | |
| Oil HHV Btu/bbl | | | | | | | | |
| ms T | 900.1 | 297.93 | (0/4,7 | 8.51101 | 1009,1 | 10/0/0 | | |
| T #124 | \$ 000 | 022.17 | 4,300 | 9002 | 1 1700 | 0 7 00 | | |

| | | | | Outputs | | | | |
|------------------|----------|-----------|----------|---------|---------|-------------------------|-----------|--|
| Corr Gross MW | 24/12 | 370.79 | 4711.2 | 480.46 | 681,76 | 875 62 | 17871 | |
| Corr Net MW | 347,23 | 346,49 | 450.0 | 454,66 | 100 N | 51777 | 1 | |
| Test Net Ht Rate | 65511 | 65711 | 08301 | 10000 | 11880 | 10000 | | |
| Corr Net Ht Rate | 11801 | 11400 | > PB01 | 10 K 20 | 10/2/01 | 0000 | 10001 | |
| Heat In MMBtu | 4021.040 | 3970, 287 | 4925,064 | 49.00 | 1 | 101111 2000 00 00 00 | 1457 1000 | |
| Test Net MW | 354.5 | 352,7 | 454,8 | 460.2 | Т | 60000 | 0000 | |
| | 1 2 2 | | | | | 1 | 13001 | |

COAL HEAT RATE TEST DATA

| | 135.50 | , | 1/14011 | おころのクレ | 128 | 0380 | 5,23 | 128.88 | 99.16 | 79,84 | 90.16 | 1048820 | 8525 | | | |
|-------|-----------|------------------------------|----------|--------------------------|----------|--------|-----------|------------------|-----------------|------------|------------|---------------|-----------------|--------------|-----------------|--|
| | (34.79 | | 46/0/12 | 1850A77 | 200 | 37.8 | 5.14 | 128,06 | 98,80 | 18.84 | 89,26 | 104/400 | 12/3 | | | |
| | 120.99 | | 79/0/17 | 2750897 | 767 | 33,0 | 4.17 | 120.85 | 94,84 | 74.46 | 18.48 | 9080 | 8726 |) | | |
| | 120.57 | tions | 26/01/2 | 7940278 | 166 | 33.7 | 4,13 2.36 | 120.30 | 94,21 | 72.52 | 74.51 | 24140 | 8744 | | | |
| | 105.31 | Data Needed For Calculations | 46/01/2 | 2250897 | 280 | 24 | 2.10 2cm | 18.02 | 59,46 | 81:12 | 72,35 | 345300 | S885 | | | |
| | 1.6. 1.11 | Data Ne | 7/10/197 | 2250A97 | 276 | 24 | Lell 2.07 | (20.12 | 85,58 | 10.97 | 72,52 | 34/400 | 2885 | | | |
| | 13500 | | 7/9/97 | 2450897 | 682 | 29.9 | 3,65240 | 110,60 | 92,24 | 72.98 | 75,29 | 780200 | 8643 | | | |
| | | | 1/9/97 | 2650 A97 | (1855 | 30,1 | 367 237 | 116,82 | 94,40 | 1/6/1 | 73.24 | 791300 | 5089 | | | |
| Unit: | | | Date | File Name , DAT 2650 AG7 | Gross MW | Aux MW | | Circ Water Out T | Circ Water In T | Wet Bulb T | Dry Bulb T | Coal Flow pph | Coal HHV Btu/lb | Oil Flow bph | Oil HHV Btu/bbl | |

| | | | | Outputs | | | | |
|------------------|-----------|-----------|----------|-----------|---------|-----------|-------------------|---------|
| Corr Gross MW | 679.37 | 677,44 | 271.17 | 91/508 | 786.3 | 1,687 | 11:168 | 893,13 |
| Corr Net MW | (049.27 | 647,54 | 247, (7 | 01.150 | 753,2 | 1.254 | 18.858 | 855:13 |
| Test Net Ht Rate | 10499 | 10341 | 12021 | 11917 | 10357 | 10437 | | 10482 |
| Corr Net Ht Rate | 10590 | 10414 | 2727 | 12147 | 10422 | 10477 | 10447 | 10456 |
| Heat In MMBtu | 6875,4057 | 6743,2686 | 2033.339 | 3050,7255 | 184048K | 7921.4638 | 168 7172,2175 891 | 8941.02 |
| Test Net MW | Q54.9 | 452.1 | | 256 | 757.9 | 0 | 852,2 | 8530 |
| | | | | , | | | { } | |

H. I. = 912.708 + 8.392(NMW) + ,001138(NMW)

COAL HEAT RATE TEST DATA Con Cool. = 47,739

404 Fr = 993.81896+ 7.3926156(MW) + 4.062342624(MW)

| 7-21-98 | | | | Data N | Data Needed For Calculations | ations | | | |
|--|-----------------|------------|----------|----------|------------------------------|---------|----------|----------|----------|
| w8145ca. w81525a. w81525b. w816acua. 474 475 557 559 624 0765 474 475 557 559 624 0765 31.0 31.1 31.7 35.2 35.2 35.7 T 10.46 10.37 17.31 116.44 114.94 T 40.46 17.74 17.77 14.94 14.94 T 75.36 75.74 72.01 73.17 74.25 74.57 T 75.15 76.73 75.73 76.12 Mb 55770 5580 63610 72020 7440 Wb 5593 8590 8590 8590 | Date | 1-21-98 | 86-12-6 | 86-22-6 | 25-25-6 | 86-82-6 | 7-23-98 | 25-77-6 | 26-75-7 |
| ### 475 \$57 \$59 G2G ONTGES \$1.0 \$1.1 \$1.7 \$1.5 \$3.2 \$3.2 \$3.2 \$3.7 \$1.5 \$1.5 \$3.2 \$3.2 \$3.7 \$3.69 \$3.7 \$1.5 \$3.2 \$3.2 \$3.7 \$1.5 \$3.2 \$3.7 \$1.5 \$3.2 \$3.7 \$1.5 \$1.5 \$3.2 \$3.7 \$1.5 \$1.5 \$1.5 \$3.69 \$1.5 \$1.5 \$1.5 \$1.5 \$1.5 \$1.5 \$1.5 \$1.5 | File Name | con81450a. | we14506. | 252525A. | W815256. | 2 | WR1600b. | WB1680a. | W816806. |
| ## \$21.0 \$1.1 \$1.7 \$1.5 \$3.2 \$3.2 \$3.2 \$3.2 \$3.2 \$3.2 \$3.2 \$3.2 | Gross MW | 474 | 475 | 557 | 828 | めいり | 0/7/0/8 | 712 | 712 |
| Ess 2.95 3.22 3.27 3.69 3.71 T 1/0.46 1/0.57 (12.41 1/3.17 1/0.44 1/4.94 T 96.04 95.86 94.75 96.35 96.35 T 75.36 75.74 72.01 73.77 74.25 74.37 T 75.36 75.73 75.52 76.73 76.73 76.73 In 55770 55780 63.800 636.00 72020 71440 In 5593 8593 8590 8590 In 40 8553 8590 | Aux MW | 31.0 | 31.1 | 21.2 | W 21.00 | とみなり | WW W | えがい | 35,8 |
| T 1/0.46 710.37 (12.91 113.17 (16.44 114.94.) T 96.04 95.86 94.75 95.17 96.35 96.35 T5.36 75.74 72.01 73.17 74.25 74.37 T5.36 75.78 75.73 75.52 76.12 Mb 557700 557800 652800 636100 720200 714400 Mb 8595 8486 8534 8449 8585 8590 | Cond Back Press | 3,95 | 2,8 | 3,22 | 3,27 | 3,69 | 3.71 | 3,77 | 3,74 |
| T 96,04 95,86 94,75 95,17 96,35 96,33 14,37 75,36 75,74 73,01 73,77 74,23 74,37 74,37 74,37 76,12 16,1 | Circ Wtr Out T | 110,46 | 110,37 | 1677) | 113.17 | 1/6,4 | 114,94 | 1/8/7 | 118,09 |
| 75,36 75,74 72,01 73,17 74,25 74,37 75,37 75,22 76,12 75,15 75,52 76,12 75,73 75,52 76,12 75,73 75,52 76,12 75,52 76,12 75,52 76,12 75,52 76,12 75,52 76,1 | Circ Water In T | 96,04 | 95,86 | 54,75 | 62:17 | 96,35 | 96,33 | 94,63 | 94,26 |
| ## 557700 557800 635800 636700 720200 714400 ### \$557700 557800 635800 636700 720200 714400 #### \$5595 \$486 \$534 \$449 \$555 \$590 ################################### | Wet Bulb T | 75.36 | 75,74 | 1018/ | 013.10 | 74,23 | 74,37 | 15,94 | 13,28 |
| In \$577700 \$57800 \$3800 \$36100 720200 714400 Wilb \$395 \$456 \$534 \$449 \$553 \$590 bbi \$10 \$10 \$10 \$25 \$590 | Dry Bulb T | 78.15 | 75.78 | 66.27 | 75.73 | 75,52 | 76,12 | 00.5% | 74,02 |
| will 8593 8486 8534 8449 8583 8590 bbi 410 416 41 | Coal Flow pph | 557700 | 557800 | 032800 | 036100 | 72020 | 714400 | 826000 | 824000 |
| bbl 445 447 605 818 602 888 | Coal HHV Btu/lb | 8393 | 8486 | \$558 | 8449 | XXXXXX | _ | からの火 | インジン |
| 415 ANS ANS ANS ANS | Oil Flow bph | | | | | | | | |
| AND AND ROP NOW MAKE | Oil HHV Btu/bbl | | | | | | | | |
| | EMO | 435 | 146 | いたり | 878 | 593 | 383 | 675 | 6.76 |

| | | | | Outputs | | | | |
|------------------|----------|---------|---------|---------|---------|----------|----------|---------|
| Corr Gross MW | 52027 | 473,2 | 551,34 | 554,13 | 622.00 | 1018,02 | 208.29 | 18 606 |
| Corr Net MW | 440,25 | 442,1 | 519,64 | 522,68 | 558,86 | 579,82 | 672,79 | 15/120 |
| Test Net Ht Rate | 105661 | 10663,4 | 10280,4 | 10/88/5 | 10427.6 | 10511.6 | 10462,7 | 10424,7 |
| Corr Net Ht Rate | 10632.0 | 10706,7 | 10392,3 | 10283,5 | 10497.4 | 1/25/2/ | 105201.3 | 270501 |
| Heat In MMBtu | 41080,77 | 4733,49 | 5400,31 | 537440 | 6/8/.47 | 6126.109 | 007707 | 0088,91 |
| Test Net MW | 4430 | 443.9 | 525.3 | 527.5 | 862,8 | 583,8 | 676,5 | 476,2 |
| | | | | | | 6.11.60 | | |

Claim Withdrawn. Contains No CBI. 06/29/2016_YD

Unit:

COAL HEAT RATE TEST DATA

| | | | Data N | Data Needed For Calculations | ations | | | |
|-----------------|--------------|--------------------|---------------------|--|-------------------|-----------|---------|----------------------|
| Date | 86-572 | 7-25-98 | 7-22-98 | 86-27-4 | 86-82-4 | 2027 | 7.21-98 | 72/-8 |
| File Name | P. BUILM IBW | + LUBS ENTINANCE + | WOLWENDER OF 1225a. | 11/K1225h. | WA12256. WE13000. | 11181300K | | 11/8/12/8/ |
| Gross MW | 192 | 192 | 247 | 247 | 3.28×26 | X7X | 1000 | 2004 2004 2004 |
| Aux MW | 28.3 | 78.1 | 768 | 7.8% | 80.08 | 20.0 | 20,2 | V 200 |
| Cond Back Press | 200 | 8,8 | 18.8 | 40.00 | 2.57 | 0.00 | 0/8/0 | 200 |
| Circ Wtr Out T | 16.71 | 66.17 | 101,26 | 101,29 | 16751 | 104/60 | 178,30 | 18.80 18.80 |
| Circ Water In T | 90.26 | 89,52 | 89,56 | 90,22 | 82.06 | 18'01 | 92,26 | 95.13 |
| Wet Bulb T | 13.99 | 73,73 | 74.85 | 73.61 | 73,84 | 74,66 | 6656 | 15 31 |
| Dry Bulb T | 1651 | 76'56 | 79,21 | 77.52 | 75,42 | 76,97 | 81,23 | 19.75 |
| Coal Flow pph | 267000 | 200300 | 3/4000 | 2/4200 | 5 | こうなみか | 473600 | 478/00 |
| Coal HHV Btu/lb | 8430 | 8419 | 8/0/2 | \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | +- | いいない | 0128 | 0/20 |
| Oil Flow bph | | | | A CONTRACTOR OF THE CONTRACTOR | | | 7 | 700 |
| Oil HHV Btu/bbl | | | | | | | | |
| USH J | | 200 | 0)/5 | 21.0 | 2005 | 650 | 4/0 | 269 |
| | | | | - | 20 0 | | 050 | • |

| | | | | Outputs | | | | |
|------------------|-----------|----------|-----------|---------|---------|----------|---------|---------|
| Corr Gross MW | 189,24 | 12.681 | 244,80 | 244,19 | 78 768 | 827. 12 | 204 2C | 201. 21 |
| Corr Net MW | 160,94 | 11.11.01 | 21842 | 010 10 | 201 24 | 100/ 200 | ひく ひこか | 2/0/2/ |
| Test Net Ht Rate | 125/10/10 | 0 20001 | 270701 | 11/00/ | 10000 | 12 K | いっつううこ | 70000 |
| Corr Net Hr Rate | 1/2001 | 00/00/ | 0/2/2/ | 1401/10 | 11001 | 1101011 | (12250) | 40000 |
| | 6,000 | | 11100 111 | 1 | 1133211 | 114501 | 1104911 | (10640) |
| Heat In MMBtu | 12200 | 7 | 2706.05 | 3 | 3374,77 | 3398,62 | 4024.59 | 1274 |
| Fest Net MW | 165.7 | 163,9 | 217.6 | 218.3 | 300.4 | 238.7 | 366,8 | 368,5 |
| | | | | | 222,84 | | | |

COAL HEAT RATE TEST DATA

Plant: VIIITE IN MAN

| | | | Data N | Data Needed For Calculations | tions | |
|-----------------|-----------|---------------|-----------|------------------------------|-------|--|
| Date | 8-72-6 | 85-75-6-6 | 86-75-6 | 86-75-4 | | |
| File Name | WR171609. | UN34 Mel. 15. | CUB1815a. | + | | |
| Gross MW | 0.80 | 4 | X V V V | N N N | | |
| Aux MW | 300° 7 | 5.50 | 0.6% | 100 N | | |
| Cond Back Press | 4.10 | 4,13 | 4.60 | 4,7/ | | |
| Circ Wtr Out T | 120.87 | 121.49 | 123.66 | 124.80 | | |
| Circ Water In T | 48,82 | 05,17 | 64,26 | 24,54 | | |
| Wet Bulb T | 72,50 | 12.61 | 20.00 | 17.00 | | |
| Dry Bulb T | 73,12 | 14,64 | KY TX | N. S. | | |
| Coal Flow pph | 933400 | 94480 | 1021/201 | 10/00/01 | | |
| Coal HHV Btu/lb | 8408 | X4X | の次が次 | 2000 2000 | | |
| Oil Flow bph | | | | | | |
| Oil HHV Btu/bbl | | | | | | |
| £ 1/15 | La Cala | 654 | 201.00 | 200 | | |
| | | | | | | |

| Outputs | \ <u>\</u> | | | | | V.Z.S. | |
|---------|----------------------|---------------------|--------------------------|--------------------------|-------------------------|--------------------|--|
| | | 753, 62 816,0 | 10501 10500 | | 1950, 40 REGELOU | 757.4. 816,0 | |
| | Our Gross MW 791, 22 | orr Net MW 752, 522 | Fest Net Ht Rate 1030312 | Corr Net Ht Rate 10429,0 | leat In MMBtu 7848、02 | Fest Net MW フミスミ | |



Inter-Office Correspondence

TO:

Etienne Senac James Marbury Tom Schnatz George Eubanks Al Ralston

Tim Gautreau
Henry Thompson
David Harris - AECC

FROM:

Roger Lawson

DATE:

October 13, 1998

SUBJECT:

1998 White Bluff Heat Rate Test Results

Heat rate tests were performed on both White Bluff Units during the months of July and August. Co-owners were notified prior to the testing and representatives from Arkansas Electric Cooperative Corporation were present to observe. Testing was performed as required by the Entergy Heat Rate Testing Procedure for Fossil Units.

Both units were tested from minimum to maximum loads. The Unit One heat rate is slightly improved below 350 MW and slightly worse above 350 MW compared to 1997. Unit Two is improved below 450 MW and worse above 450 MW compared to 1997.

The coefficients for the 1998 heat rate curves are:

| Term | Unit 1 | Unit 2 |
|--|------------------------------|------------------------------|
| $egin{array}{c} X^2 \ X^1 \ X^0 \end{array}$ | 0.002343 7.393 993.819 | 0.001771 8.092 907.723 |

The measured heat input at each of the corrected test loads is shown in the following table.

| Unit 1 | Unit 1 | Unit 2 | Unit 2 |
|----------------|------------|----------------|------------|
| Corrected Net | Heat Input | Corrected Net | Heat Input |
| Test Load (MW) | (MMBtu/Hr) | Test Load (MW) | (MMBtu/Hr) |
| 160.94 | 2250.81 | 162.37 | 2235.64 |
| 161.11 | 2241.97 | 162.50 | 2276.15 |
| 215.42 | 2706.05 | 228.15 | 2853.21 |
| 215.49 | 2688.92 | 229.95 | 2838.88 |
| 296.82 | 3398.62 | 304.86 | 3516.07 |
| 297.24 | 3374.77 | 307.00 | 3617.44 |
| 365.15 | 4034.59 | 363.81 | 4121.70 |
| 365.81 | 4047.37 | 363.81 | 4121.70 |
| 440.25 | 4680.77 | 452.62 | 4969.72 |
| 442.10 | 4733.49 | 454.10 | 4946.59 |
| 519.64 | 5400.31 | 524.90 | 5564.15 |
| 522.63 | 5374.40 | 524.93 | 5571.39 |
| 579.83 | 6136.69 | 681.61 | 7261.24 |
| 588.86 | 6181.47 | 685.72 | 7327.80 |
| 671.51 | 7055.91 | 822.51 | 8721.82 |
| 672.79 | 7077.99 | 822.80 | 8801.52 |
| 752.52 | 7848.02 | | |
| 753.62 | 7950.49 | | |
| 813.52 | 8520.24 | | |
| 816.00 | 8567.97 | | |
| | | | |

The results have been reviewed and approved for implementation by James Marbury.

The complete test results are presented as charts in the \underline{EXCEL} spreadsheet "WBHR1998.XLS" which is provided as an attachment to this memo.

cc: Pat Klepper

COAL HEAT RATE TEST DATA

| | | | | Data Needed For Calculations | ations | | | | |
|------------------|---------|---|-------------|------------------------------|----------------|-------------|-----------------|-----------------|------------|
| Date | 8677 | 862-1, | 86-87 | 86-87 | タンプ | あるカー | 7988 | 80-07 | |
| File Name | 294500. | 182708 | 1000 B | Sangy. | 20/200, | 20000 | 2021/10. | 22 to 1/6, | |
| Gross MW | 473 | 477 | 1257 | 550 | 7/0 | 7/2 | 858 | 855 65 | \bigcirc |
| Aux MW | 24,9 | 0 2 2 2 3 3 4 3 4 3 4 3 4 3 4 3 4 3 4 3 4 | 700 | 25.8 | \$\land{\pi}\$ | M O M | 8 1/2 1/2 | 428 | <u> </u> |
| Cond Back Press | 500 | 3129 | 3,59 | 0 iv | 4,42 | 4,40 | 5,34 | 5,36 | |
| Circ Water Out T | 11000 | 11/87 | 114,25 | 1/4.29 | 1/8/2/ | 118,54 | 124,03 | 124,65 | |
| Circ Water In T | 34.70 | 07.26 | 95,32 | 95,85 | 17'76 | 1.17.75 | 95.04 | 70°04 | |
| Wet Bulb T | 0/32 | 74.22. | 8/12 | 78,22 | 20,0% | 81,82 | 8212 | 77,25 | |
| Dry Bulb T | 61.11.8 | 97:16 | 80.78 | 97,76 | 870,82 | 18/8 | 18.91 | 78,23 | |
| Coal Flow pph | 55250 | 55.158V | 000000 | 033400 | 34620C | 844600 | 2007/0/ | 10/9500 | |
| Coal HHV Btu/lb | 870 | 2250 | NO STATE OF | 3678 | \ W.W.W. | めるとい | 15/32V | マシスタイ サ タSSド | |
| Oil Flow bph | | | | | | | | 1 | |
| Oil HHV Btu/bbl | | | | | | | | | |
| EMO | | | | | | | 822 | 22.10 | |
| | | | | | | | | | ~~~ |
| | | | | Outputs | | | | | ** |
| Corr Gross MW | 0.667 | 477,62 | / NN/ | 00000 | 161114 | 716.02 | めこと | 16758 | W |
| Corr Net MW | 4541 | 432,00 | か、ケスペ | 824 BB | 15789 | (085,72 | かってか | 822,5/ | |
| Test Net Ht Rate | 23801 | 250011 | 10000 | 87907 | 10083 | 10749 | 10001 | 0650/ | |
| Corr Net Ht Rate | 12822 | 10980 | 16 600 | 10014 | 85001 | 2820/ | 1.0001 | 4000/ | |
| Heat In MMBtu | 1446.57 | tx1.6967 | 2004. IN | 7547455 | 7201,242. | 02811820 | 6/5/088 | 872/.823 | · } |
| Test Net MW | 1.7 | 4520 | 4. K. | してです | 1079.7 | 7.100 | 820.8 | 1000 DOV | V (|

COAL HEAT RATE TEST DATA

8,83 23.7 3800 23.0 308 330 402 Data Needed For Calculations Oil Flow bph Oil HHV Btu/bbl Coal HHV Btu/lb Cond Back Press Circ Water Out T Circ Water In T Coal Flow pph Wet Bulb T Dry Bulb T File Name Gross MW Aux MW

| | | | | Outputs | | | | |
|------------------|-----------|---------|--------------|-----------------------------|----------|----------|----------|--|
| Corr Gross MW | 5 X/ | 184,97 | 252.05 | 250,75 | 32728 | 830,0 | 151288 | |
| Corr Net MW | 11.50/ | 162.33 | 20,27 22,000 | 228,15 | 304,86 | 30%0 | 363.81 | |
| Test Net Ht Rate | 14007.1 | 964581 | (2532 | 12492 | 11555 | 11783 | 11345 | |
| Corr Net Ht Rate | 1.1.2.361 | 13769 | 12346 | 12,506 | 11533 | 11755 | 11329 | |
| Heat In MMBtu | 22.26.149 | 2235.40 | | 2853,214. 3516,073 3417,410 | 35/6,073 | 3617,410 | 4(21,047 | |
| Test Net MW | 162,5 | 1102,4 | 230,2. | 228,4 | 304.3 | 30% | 363,3 | |

gwbosic. ore

0 = 7,464

COAL HEAT RATE TEST DATA

Plant: CUD

Unit:

| | | | Data N | Data Needed For Calculations | ations | | | |
|------------------|---------|----------|---------|------------------------------|--|----------------|---|--|
| Date | 86/00/8 | 86/02/8 | 8//7 | 8/17 | 2//2 | 8/17 | RIS | 8/20 |
| File Name | 26 1600 | 23/606. | 262254. | 18258 | 263000. | 2630b. | 263759. | 263756. |
| Gross MW | 021 | 56/ | 246 | 24.6 | 326 | 324 | 294 | 394 |
| Aux MW | 22,6 | 22.8 | 18.1 | 621 | 15.9 | 18,7 | 24.8 | 24.6 |
| Cond Back Press | 2,05 | 4.03 | 2,23 | 8,80 | 2,64 | 2.62 | 71/ | 2,70 |
| Circ Water Out T | 98,74 | 18186 | (01,27 | (CD), 84 | 106.43 | 106.18 | 105,49 | 18'501 |
| Circ Water In T | 5206 | 95'06 | 96't8 | 84,52 | 18:58 | 85,73 | 4016 | 90,90 |
| Wet Bulb T | 176,60 | の名がろ | 68.4S | 07.69 | 69,88 | 08,80 | 1,0,01 | 18:00 |
| Dry Bulb T | 81.67 | 28.35 | 70,37 | 081/2 | 70,88 | 70,73 | 14144 | 486 |
| Coal Flow pph | 272200 | 001.11.0 | 336000 | 33338 | 42360 | 421400 | 8838 | 2000 |
| Coal HHV Btu/lb | 8562 | 8476 | 8328 | 8473 | 8958 | 8500 | 7C78 | C 7504 |
| Oil Flow bph | | | Love wh | 04 W 60 | A) A A A A A A A A A A A A A A A A A A | Carried States | CONTRACTOR OF THE PARTY OF THE | and the second s |
| Oil HHV Btu/bbl | | | | | | | | |
| | | | | | | | | |

| | | | | Outputs | | | | |
|------------------|---------|---------|----------|---------|--------|---------|---------|---------|
| Corr Gross MW | 175.70 | 85'841 | 239.08 | 14.656 | 319,64 | 60718 | 389,13 | 16,688 |
| Corr Net MW | 153.10 | 82.051 | 220,98 | 181166 | 200,74 | 66'868 | 364.33 | 15:598 |
| Test Net Ht Rate | 15/93 | 18/31 | 12323 | 12477 | 8/8// | 11732 | 11621 | 18611 |
| Corr Net Ht Rate | EZZS1 | 15274 | 80181 | 15821 | 12068 | 0.86// | 11776 | 12115 |
| Heat In MMBtu | 2330,58 | 2302.83 | 62.808.0 | 2846,08 | 202940 | 3581.90 | 4290.34 | 4425,73 |
| Test Net MW | 153.4 | 152,2 | 61288 | 13281 | 307.1 | 305.3 | 369,2 | 369,4 |
| | | | | | | | | |

COAL HEAT RATE TEST DATA

Unit:

| | | | Data N | Data Needed For Calculations | lations | | | |
|------------------|---------|---------|----------|------------------------------|-----------|---------|---------|---------|
| Date | 34/8/18 | 2//8 | 8//8 | 2//8 | 8/29 | 8/29 | 8/19 | 8/18 |
| File Name | 2645000 | 26450b. | 26525a. | 265256. | 26,600 a, | 2600060 | 266809. | 26080b. |
| Gross MW | 478 | 924 | 848 | 550 | 180 | 050 | 11/2 | 712 |
| Aux MW | 6.55 | 25.8 | 26.6 | 20,5 | 29,5 | 29.3 | 30,8 | 30,7 |
| Cond Back Press | 305 | 3,01 | 3,19 | 21/15 | 3,66 | 3,63 | 4.09 | 4.05 |
| Circ Water Out T | 108.72 | 168.38 | 109,56 | 16'801 | 1/3.46 | 60'811 | 05'711 | 116.17 |
| Circ Water In T | 6676 | 5116 | Cb'06, | 98.06 | 22.22 | 11126 | 73.62 | 13127 |
| Wet Bulb T | 73,2 | 72,73 | p6'02 | 18181 | 12,97 | 73,97 | 70125 | 73,40 |
| Dry Bulb T | 16.73 | 01191 | 72,42 | 74.71 | 75.09 | 75.66 | to 1/2 | 74,18 |
| Coal Flow pph | 01/845 | 276200 | COS/100) | 040400 | 770300 | 773000 | 863.320 | SOTE |
| Coal HHV Btu/lb | 0948 | 00t8 | 8425 | 8476 | 9758 | 6118 | 268 | 8541 |
| Oil Flow bph | | | | - | | | | |
| Oil HHV Btu/bbl | | | | | | | | |
| - | | | | | | | | |

| | | | | Outputs | | | | |
|------------------|---------|---------|---------|---------|--------|----------|---------|--------|
| Corr Gross MW | 473.56 | 501127 | 541,65 | 544,73 | 21:20 | G200: 12 | 702,64 | 86.50% |
| Corr Net MW | 447,66 | 445.85 | 50/5/5 | 57815 | 597.62 | 280,82 | 481/29 | 675,28 |
| Test Net Ht Rate | 10818 | 15201 | 6/401 | 10466 | 90601 | 10445 | 10657 | 51801 |
| Corr Net Ht Rate | 10925 | 10856 | 10547 | 10572 | 11097 | 5/50/ | 06601 | 10972 |
| Heat In MMBtu | 4890.73 | 4840.08 | 5432.44 | 5478.89 | 183859 | 4274.44 | 7249,13 | 740932 |
| Test Net MW | 17231 | 450.2 | 4128 | 523,5 | (401.5 | 4000,7 | 680,2 | 681.3 |

COAL HEAT RATE TEST DATA

| | | | | | , | | | | | | | | | |
|------------------------------|-------|-----------|----------|--------|-----------------|------------------|-----------------|------------|------------|---------------|-----------------|--------------|-----------------|--|
| | | | | | | | | | | | | | | |
| tions | | | | | | | | | | | | | | |
| Data Needed For Calculations | 18/18 | 26/20116. | 14.8 | 320 | 0,10 | 18:88 | 9343 | 72,34 | 6577 | 00/100/ | 8364 | | | |
| Data N | 6/18 | 28 Killa. | 168 | 36,7 | 5.13 | 123.04 | 93,56 | 78.5 | 11/2 | 0000001 | 8403 | | | |
| | 8/20 | 267606. | 295 | 34, 1 | 4.01 | 40.00 | 93.54 | 75.20 | 78,29 | 20,6266 | 2618 | | | |
| | 8/29 | 22.7600. | 866 | 33.7 | 6517 | 76'611 | 93,52 | 18,41 | 91156 | 970300 | 5828 | | | |
| | Date | File Name | Gross MW | Aux MW | Cond Back Press | Circ Water Out T | Circ Water In T | Wet Bulb T | Dry Bulb T | Coal Flow pph | Coal HHV Btu/lb | Oil Flow bph | Oil HHV Btu/bbl | |

| | | | | Outputs | | |
|------------------|---------|--------|---------------|-----------------|--|--|
| Corr Gross MW | 02787 | 66766 | 266,79 804,76 | 804,76 | | |
| Corr Net MW | 001256 | 197.67 | 830,09 | 9/2/2/28 | | |
| Test Net Ht Rate | 10049 | 98501 | 10717 | 1082 | | |
| Corr Net Ht Rate | 57701 | 1.8501 | 10771 | 78201 | | |
| Heat In MMBtu | 8085,5Y | 1 | 8940.79 | 8940.79 8925,22 | | |
| Test Net MW | 5.656 | 760.9 | 834.3 | 834.0 | | |



June 2, 1993

Inter-Office Correspondence

TO:

Mr. Art Gilreath

FROM:

Dennis A. Wall

SUBJECT:

1993 Maximum Operating Ratings Tests: White Bluff Plant

The purpose of the subject tests was to determine the present full load ability of the White Bluff units when operating at a weather condition equal to the past five years' average maximum daily wet bulb temperature of 76 °F. The tests and related calculations have been completed, and the results are attached for your review. Both unit's tests were conducted in accordance with the relevant Entergy test procedure.

The Unit 1 test was conducted on May 12th. The test went normally and resulted in a full load capability of 801 MW, which is 14 MW less than its MDC rating. The limitation was due to "B" PA Fan air flow.

The Unit 2 test was conducted on May 13th. The test went normally and resulted in a full load capability of 833 MW, which is 11 MW less than its MDC rating. The limitation was due to "A" ID Fan suction pressure.

Denno a. Wall

If you need any additional information, please contact me at extension 7021.

DAW/dw

cc:

Mr. Mickey Cox

Mr. Max Halbert

Mr. Tom Odenthal

Mr. Ron House

Mr. Gary Davis

White Bluff Plant Unit 1

Maximum Operating Ratings Calculations

MDC CORRECTIONS FOR WHITE BLUFF - 1

BACKPRESSURE CORRECTION RESULTS FOR WHITE BLUFF - 1

| Cooling Tower Circulating Water Flow Rate 341000 Cooling Tower Range 26.94 | חדכ ב |
|--|----------|
| Design Maximum Cold Water Temperature | DEG F |
| Test Backpressure | |
| Test Backpressure to 4.5 In-HG | % |
| AMCCWT Saturation Pressure to 4.5 In-HG | 8 |
| Change in KW Load from Test to AMCCWT Backpressure | |
| BACKPRESSURE CORRECTION DIVISOR | 8 |
| | |

INITIAL TEMPERATURE CORRECTION RESULTS FOR WHITE BLUFF - 1

HOT REHEAT TEMPERATURE CORRECTION RESULTS FOR WHITE BLUFF - 1

| The Test HRH Temperature was within In accordance with the Entergy Test BE MADE IN THIS CASE. | 1% of the design value (1000 F). Guidelines, NO CORRECTION WILL |
|---|--|
| Change in KW Load for Hot Reheat Tem | perature 0.00 % |
| HOT REHEAT TEMPERATURE CORRECTION DI | VISOR 1.0000 |

SUMMARY OF CORRECTION CALCULATIONS FOR WHITE BLUFF - 1

| Product of Correction Factors | 1.0167 |
|---|------------------------|
| Test Gross Generation | 852.50 MW 838.47 MW |
| Test Net Generation | 814.90 MW 800.87 MW |
| MAXIMUM CAPABILITY (per summer test guidelines) | 801 MW |

White Bluff Plant Unit 2

Maximum Operating Ratings Calculations

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MDC CORRECTIONS FOR WHITE BLUFF - 2

| MEASURED TEST INPUTS FROM FILE w2051393.mdc | |
|---|---------------------|
| | |
| Average Gross Generation | MWe MVAR PSIC |
| Average Condenser Vacuum 26.00 Average Barometric Pressure 29.50 | IN-HG |
| Average Hot Water Temperature from the Condenser 114.63 Average Cold Water Temperature to the Condenser 87.04 | DEG F |
| Average Ambient Wet Bulb Temperature | DEG F DEG F |
| Average Turbine Throttle Flow Average Initial Pressure | LBM/HR |

BACKPRESSURE CORRECTION RESULTS FOR WHITE BLUFF - 2

| Cooling Tower Circulating Water Flow Rate 341000 Cooling Tower Range 27.59 | GPM | 179 |
|---|-----|-----|
| Design Cold Water Temperature | DEC | E |
| Test Backpressure | | |
| Test Backpressure to 4.5 In-HG | ş. | G |
| AMCCWT Saturation Pressure to 4.5 In-HG0.22 Change in Heat Rate from Test to AMCCWT Backpressure 1.11 | 8 | |
| Change in KW Load from Test to AMCCWT Backpressure1.10 | | |
| BACKPRESSURE CORRECTION DIVISOR 1.0110 | ક | |
| | | |

The Test Initial Pressure was greater than the 5 % overdesign value (2520 psig). This is above the recommended operating range for this unit (per General Electric). Correction from the test value down to the 5 % overdesign value will cause a decrease in capability. In accordance with the Entergy Test Guidelines, THIS CORRECTION WILL BE MADE.

Reference General Electric Drawing GEZ-3614

| Change in KW Load from Test to Standard Initial Pressure | 5 10 | 9- |
|---|------|----|
| Change in KW Load from 5% Overpressure to Standard Initial Pressure | | |
| Change in KW Load from Test to 5% Overpressure | | |
| INITIAL PRESSURE CORRECTION DIVISOR | | |

The Test Initial Temperature is less than the design value (1000 F), by more than 1%. Correction upward would cause a decrease in unit capability. In accordance with the Entergy Test Guidelines, THIS CORRECTION WILL BE MADE.

Correction will be made from the Test Initial Temperature of 982.65 F to the corrected value of 990 F (the lower limit of the 1% margin allowed by the Entergy Test Guidelines.

Reference General Electric Drawing GEZ-3615

| Change in KW Load from Test to Standard Initial Temperature | 0 17 % |
|--|--------|
| Change in KW Load from 990 F to Standard Initial Temperature | |
| Change in KW Load from Test to 990 F Initial Temperature | |
| INITIAL TEMPERATURE CORRECTION DIVISOR | |

HOT REHEAT TEMPERATURE CORRECTION RESULTS FOR WHITE BLUFF - 2

| The Test HRH Temperature was within 1% of the design value (1000 F). In accordance with the Entergy Test Guidelines, NO CORRECTION WILL BE MADE IN THIS CASE. |
|---|
| Change in KW Load for Hot Reheat Temperature 0.00 % |
| HOT REHEAT TEMPERATURE CORRECTION DIVISOR 1.0000 |

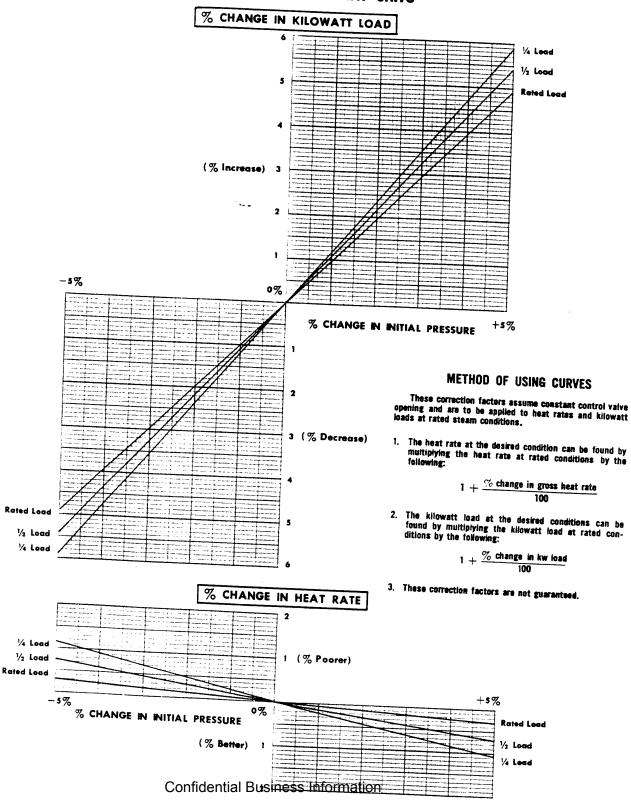
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SUMMARY OF CORRECTION CALCULATIONS FOR WHITE BLUFF - 2

| Product of Correction Factors | 1.0137 |
|---|------------------------|
| Test Gross Generation | 879.00 MW 867.11 MW |
| Test Net Generation | 844.70 MW 832.81 MW |
| MAXIMUM CAPABILITY (per summer test guidelines) | 833 MW |

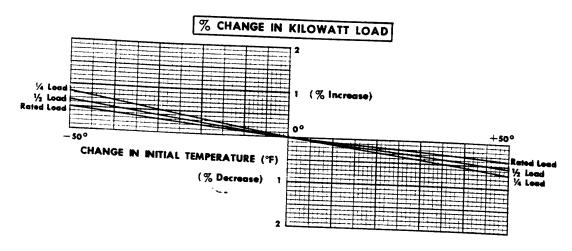
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INITIAL PRESSURE CORRECTION FACTORS FOR SINGLE REHEAT UNITS



INITIAL TEMPERATURE CORRECTION FACTORS

FOR SINGLE REHEAT - SUBCRITICAL PRESSURE UNITS



METHOD OF USING CURVES

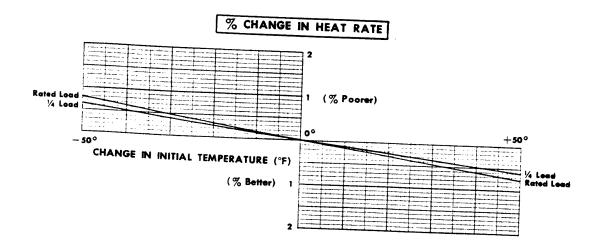
These correction factors assume constant control vaive opening and are to be applied to heat rates and kilowatt loads at rated steam conditions.

 The heat rate at the desired condition can be found by multiplying the heat rate at rated conditions by the following:

The kilewatt load at the desired conditions can be found by multiplying the kilowatt load at rated conditions by the following:

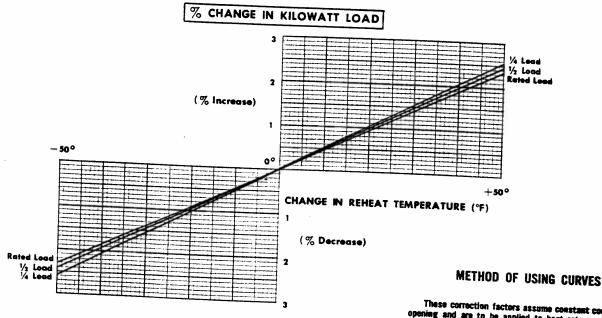
$$1 + \frac{\% \text{ change in kw load}}{100}$$

3. These correction factors are not guaranteed.



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REHEAT TEMPERATURE CORRECTION FACTORS FOR SINGLE REHEAT UNITS



These correction factors assume constant control valve opening and are to be applied to heat rates and kilowatt loads at rated steam conditions.

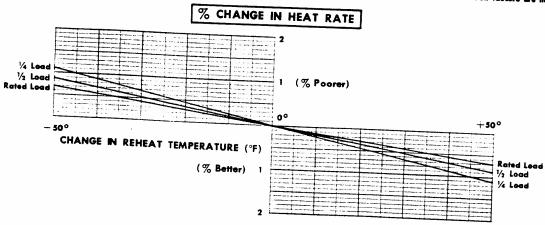
The heat rate at the desired condition can be found by multiplying the heat rate at rated conditions by the following:

$$1 + \frac{\% \text{ change in gross heat rate}}{100}$$

The kilowatt load at the desired conditions can be found by multiplying the kilowatt load at rated con-ditions by the following:

$$1 + \frac{\% \text{ change in kw load}}{100}$$

3. These correction factors are not guaranteed.



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GEZ-3617

